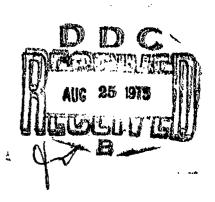
Band Model Parameters for the 2.7- μ m Bands of H_2O and CO_2 in the 100 to 3000°K Temperature Range

S. J. YOUNG Chemistry and Physics Laboratory Laboratory Operations The Aerospace Corporation El Segundo, Calif. 90245

31 July 1975

Interim Report

APPROVED FOR PUBLIC RELEASE: DISTRIBUTION UNLIMITED



Sponsored by

DEFENSE ADVANCED RESEARCH PROJECTS AGENCY 1400 Wilson Blvd Arlington, Va. 22209

DARPA Order No. 2843

SPACE AND MISSILE SYSTEMS ORGANIZATION AIR FORCE SYSTEMS COMMAND Los Angeles Air Force Station Los Angeles, Calif. 90045

THE VIEWS AND CONCLUSIONS CONTAINED IN THIS DOCUMENT ARE THOSE OF THE AUTHORS AND SHOULD NOT BE INTERPRETED AS NECESSARILY REPRESENTING THE OFFICIAL POLICIES, EITHER EXPRESSED OR IMPLIED, OF THE DEFENSE ADVANCED RESEARCH PROJECTS AGENCY OR THE U.S. GOVERNMENT.

BEST

AVAILABLE

COPY

This research was supported by the Defense Advanced Research Projects Agency of the Department of Defense and was monitored by Space and Missile Systems Organization (SAMSO) under Contract No. F04701-75-C-0076.

Approved

S. Siegel, Director

Chemistry and Physics Laboratory

REGESTION for

Approval of this report does not constitute Air Force approval of the report's findings or conclusions. It is published only for the exchange and stimulation of ideas.

the second s

Ronald C. Lawson, 2nd Lt. United States Air Force

United States Air Force Technology Development Division Deputy for Technology

A STATE OF THE STA	PARTITION OF THE PROPERTY OF T
UNCLASSIFIED SECURITY CLASSIFICATION OF THIS PAGE (When Date Entered)	cnome tens)
(REPORT DOCUMENTATION PAGE	READ INSTRUCTIONS BEFORE COMPLETING FORM
SAMSO TR -75 - 209	2. RECIPIENT'S CATALOG NUMBER
BAND MODEL PARAMETERS FOR THE 2.7-BANDS OF H ₂ O AND CO ₂ IN THE 100 to 3000 K	Interim A ()
TEMPERATURE RANGE	TR -0076(6970) -4
Stephen J./Young	F/047/01-75-C-0076/
9. PERFORMING ORGANIZATION NAME AND ADDRESS The Aerospace Corporation El Segundo, Calif. 90245	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
Defense Advanced Research Projects Agency 1400 Wilson Blvd. Arlington, Va. 22209	1/31 Jul 75 13. NUMBER OF PAGES 57 (/2)/46
14. MONITORING AGENCY NAME & ADDRESS(It different from Controlling Office) Space and Missile Systems Organization Air Force Systems Command	15. SECURITY CLASS. (of this foport) Unclassified
Los Angeles, Calif. 90045	15. DECLASSIFICATION/DOWNGRADING SCHEDULE
Approved for public release; distribution unlimite	ed .
17 DISTRIBUTION STATEMENT (of the abatract entered in Block 20, if different from	n Report)

18. SUPPLEMENTARY NOTES

The views and conclusions contained in this document are those of the authors and should not be interpreted as necessarily representing the official policies, either expressed or implied, of The Defense Advanced Research Projects Agency or the U.S. Government.

19. KEY WORDS (Continue on reverse side if necessary and identify by block number)

Absorption by CO₂ Absorption by H₂O Atmospheric Absorption

ABSTRACT (Continue on reverse side if necessary and identify by block number)

Sets of band model parameters for H_2O and CO_2 in the 2.7-4m, spectral region, and consistent for the entire temperature range from near-ambient atmospheric temperatures (~200 K) to gas combustion temperatures (~2500 K), are constructed. These constructions are accomplished by joining together band model parameters derived from the AFCRL atmospheric absorption line data compilation (LINAVE parameters) and parameters tabulated in the NASA Handbook of Infrared Radiation from Combustion Gases (NASA parameters).

DD FORM 1473

1:4575

UNCLASSIFIED

UNC LASSIFIED

RECHBITY	CLASSIFICATION	OF	THIE	DAME	197k.am	Date	R-toned
2 ECOMIT	CLASSIFICATION	Ur	1412	PHUR(IA U DU	ルギに在	ARTER OF

19. KEY WORDS (Continued)

Band Model Parameters High-Temperature Absorption

20. ABSTRACT (Continued)

The former set adequately describes the low-temperature variation of the parameters but is inadequate for some high-temperature applications. The latter set is suitable for high-temperature applications but fails for some low-temperature cases. Examples of the deficiencies of these two sets are presented by comparison with experimental absorption and emission spectra for low- and high-temperature gas samples. The adequacy of the combined band model parameter set (COMB parameters) is demonstrated by comparison with the same experimental data. Criteria for and examples of the construction of the combined sets are given, and tabulations of the parameter sets are included in an Appendix. An example of the use of the new parameter sets is given by computation of the effective transmittance of the atmosphere of a hot H_2O/CO_2 emission source viewed over a long atmospheric slant path.

CONTENTS

Ι.	INTRODUCTION						
II.	BAND MODEL PARAM	METERS	7				
	A. Band Model For	mulation	7				
		ameters from Line Data eters)	11				
	· ·		19				
	D. Evaluation of Pa	arameter Sets	20				
III.	COMBINED PARAME	TER SETS	33				
	A. General Procedu	ure	33				
	B. H ₂ O Parameter	Set (COMBH2O)	34				
	C. CO ₂ Parameter	Set (COMBCO2)	37				
IV.	ATMOSPHERIC TRAN	SMITTANCE CALCULATION	41				
APP		D COMBCO2 PARAMETER	47				
		TABLES					
ı							
1.	Line Broadening Para	meters for H ₂ O and CO ₂	17				
Ai.	Listing of COMBH2O I	Band Model Parameter Set	48				
A2.	Listing of COMBCO2 I	Band Model Parameter Set	52				

FIGURES

1.	Low-Temperature Transmission Spectra for CO ₂ in the Band Center Region	22
2.	Low-Temperature Transmission Spectra for CO ₂ in the Band Wing Region	24
3.	High-Temperature Emission Spectra for CO ₂	25
4.	Low-Temperature Transmission Spectra for H ₂ O	27
5.	Low-Temperature Transmission Spectra for H ₂ O in the Band Center Region	28
6.	Low-Temperature Transmission Spectra for H ₂ O in the Band Wing Region	29
7.	High-Temperature Emission Spectra for H ₂ O	31
8.	Variation of k (H ₂ O) with Temperature for Selected Spectral Intervals	3 5
9.	Variation of $1/\delta_e$ (H ₂ O) with Temperature for Selected Spectral Intervals	36
10.	Variation of k (CO ₂) with Temperature for Selected Spectral Intervals	38
î 1 .	Variation of $1/\delta_e$ (CO ₂) with Temperature for Selected Spectral Intervals	39
12.	Source and Transmitted Radiance Spectra for Atmospheric Slant Path	43
13.	Transmittance Spectra for Atmospheric Slant Path	44
14.	Effective Transmistance Spectra for Atmospheric Slant Path	45

I. INTRODUCTION

In a previous report, band model techniques were applied to the problem of computing the effective transmittance of the atmosphere for radiation arising from hot gaseous H₂O and CO₂ emission sources. Effects of line correlation between the emission spectra and atmospheric absorption spectra were accounted for by treatment of the entire optical path consisting of the atmospheric slant path plus the line-of-sight continuation through the source as a single, highly inhomogeneous radiating and absorbing entity. Approximations for handling the large degree of inhomogeneity caused by pressure, temperature, and species concentration gradients along such an optical path were discussed.

The single most important variable that affects the degree of inhomogeneity of the path is the temperature distribution along the path. Through the atmospheric portion of the total path, the temperature variations are slight, and for many applications, the atmosphere can be considered as isothermal. In the transition region between the atmospheric portion and the source portion of the path, and within the source portion itself, large temperature gradients can exist. The effect of these temperature gradients is introduced into the band model calculations through the temperature variation of the fundamental band model parameters that describe the absorption effects of all the spectral lines in a small spectral interval $\Delta \nu$.

In the previous work, two sets of band model parameters were employed. The set designated LINAVE was generated from the line

S. J. Young, <u>Band Model Calculations of Atmospheric Transmittance for Hot Gas Line Emission Sources</u>, TR-0075(5647)-1, The Aerospace Corp., El Segundo, Calif. (31 December 1974).

strength and width data of the Air Force Cambridge Research Laboratories (AFCRL) line atlas. ² The parameter set designated GD* was taken from the NASA Handbook of Infrared Radiation from Combustion Gases. 3 The former set was expected to be reasonably accurate for low temperatures since the AFCRL line atlas was compiled primarily for atmospheric applications. Its use at higher temperatures was demonstrated to be inadequate in the 2.7-µm band wing regions. The latter set, since it was constructed for high-temperature problems, was expected to be adequate for temperatures above about 1000°K but to be of questionable utility for low temperatures. If the problem of atmospheric transmittance could be treated in a manner in which the source emission and atmospheric absorption were discoupled processes, these existing parameter sets would be sufficient to handle transmittance computations. Since the correct account of line correlation requires the entire optical path to be treated as a single entity, however, a single set of band model parameters, applicable to the entire temperature range from atmospheric temperatures (at least as low as 200°K) to combustion gas temperatures (at least as high as 2500°K), is required.

The work described in this report is concerned with the construction of band model parameter sets for the 2.7- μ m bands of H₂O and CO₂ that

These parameters were generated by workers at General Dynamics, hence the designation GD. Most people, however, refer to these data as the NASA parameters. The latter designation will be used in the remainder of this report.

²R. A. McClatchey, W. S. Benedict, S. A. Clough, D. E. Burch, R. F. Calfe, K. Fox, L. S. Rothman, and J. S. Garing, <u>AFCRL Atmospheric Absorption Line Parameters Compilation</u>, AFCRL-TR-73-006, Air Force Cambridge Research Laboratories, Mass. (25 January 1973).

³C. B. Ludwig, W. Malkmus, J. E. Reardon, and J. A. L. Thompson, Handbook of Infrared Radiation from Combustion Gases, eds. R. Goulard and J. A. L. Thompson, NASA SP-3080, Marshall Space Flight Center, Huntsville, Ala. (1973).

are internally consistent for the temperature range from 100 to 3000 °K. Section II of this report discusses the generation of the LINAVE and NASA parameter sets and gives examples of their deficiencies. The combining of these two parameter sets to give consistent sets for H₂O and CO₂ is done in Sect. III. An example of their use in an atmospheric transmittance problem is given in Sect. IV.

II. BAND MODEL PARAMETERS

A. BAND MODEL FORMULATION

The statistical band model formulation for absorption by a random array of pressure-broadened Lorentz lines depends on the specification of three fundamental band model parameters. The mean absorption coefficient \overline{k} describes the strength of absorption effected by all the lines in a spectral interval $\Delta \nu$, the mean line-spacing parameter δ_e measures the effective average distance between adjacent lines in $\Delta \nu$, and $\overline{\gamma}$ gives the mean line width of the lines in $\Delta \nu$. For most applications, δ_e and $\overline{\gamma}$ do not need to be known individually, and the mean line width to spacing parameter

$$\beta = \frac{2\pi \overline{\gamma}}{\delta_{\mathbf{e}}} \tag{1}$$

along with \overline{k} suffices to specify the absorption characteristic of $\Delta \nu$. In general, the parameters \overline{k} and δ_e are functions of spectral position and temperature while $\overline{\gamma}$ depends additionally on the pressure and species composition of the absorbing gas.

For a homogeneous optical path and a single active gas species, the mean transmittance in $\Delta \nu$ is

$$\overline{\tau} = \exp\left(-\frac{\overline{W}}{\delta}\right)$$
 (2)

More accurately, we mean the approximation to the statistical band model in which the number of lines in an interval Δv is assumed to be infinite and for which the absorption by each line whose center occurs in Δv is complete within Δv .

where \overline{W} is the mean equivalent width of all the lines in $\Delta \nu$ and

$$\delta = \frac{\Delta \nu}{N} \tag{3}$$

is the mean line-spacing parameter. The number of lines in $\Delta \nu$ is In terms of band model parameters,

$$\frac{\overline{W}}{\delta} = \beta f(x) \tag{4}$$

where

$$\mathbf{x} = \frac{\overline{\mathbf{k}} \, \mathbf{u}}{\mathbf{\beta}} \tag{5}$$

is the dimensionless optical depth parameter. The optical depth u is the product of the total gas pressure p, the mole fraction of the active gas c, and the geometric path length L:

$$\mathbf{u} = \mathbf{p} \, \mathbf{c} \, \mathbf{L} \quad . \tag{6}$$

The curve-of-growth function f(x) depends on the line strength distribution function assumed for the lines in Δv . For equal intensity lines,

$$f(\mathbf{x}) = L(\mathbf{x}) \tag{7}$$

where L(x) is the Ladenburg-Reiche function. For an exponential distribution of line strengths,

$$f(\mathbf{x}) = \frac{\mathbf{x}}{\sqrt{1 + \frac{\pi \mathbf{x}}{2}}} \tag{8}$$

AND THE PROPERTY OF THE PROPER

while for the exponential-tailed inverse distribution, *4

$$f(\mathbf{x}) = \frac{1}{\pi} \left[\sqrt{1 + 2\pi \mathbf{x}} - 1 \right]. \tag{9}$$

These curve-of-growth functions are all defined so that $f(x) \to x$ for small x and $f(x) \to (2x/\pi)^{1/2}$ for large x. In this way, the same band model parameters are appropriate for all three distribution functions.

For application of the statistical band model to inhomogeneous optical paths, approximations must be introduced to account for pressure, species concentration, and temperature gradients along the line of sight. In both the Curtis-Godson (CG) and Lindquist-Simmons (LS) approximations, this account is made by the employment of path-averaged values of the band model parameters. For a path extending from the geometric position s=0 to the general position s along the line of sight, the appropriate path averages are

$$\overline{k}_{e}(s) = \frac{1}{u(s)} \int_{0}^{s} c(s') p(s') \overline{k}(s') ds'$$
 (10)

and

$$\beta_{e}(s) = \frac{1}{u(s) \overline{k}_{e}(s)} \int_{0}^{s} c(s') p(s') \overline{k}(s') \beta(s') ds'$$
(11)

dan sa ing panglas ing kangkarang kangkarang sang sang pangkarang kangkarang pangkarang sa sa sa sa sa sa sa s

The exponential-tailed inverse line strength distribution was invented by Malkmus (Ref. 4) as an approximation to the purely inverse line strength distribution function. The resulting curve of growth function [Eq. (9)] is substantially simpler in form than that for the inverse distribution.

⁴W. Malkmus, J. Opt. Soc. Am. 57, 323 (1967).

where

$$u(s) = \int_0^{s} c(s') p(s') ds'$$
 (12)

In the CG approximation, K_0 and B_0 are used in place of K and B_1 , respectively, in the equations for a homogeneous optical path. In the LS approximation, these path-averaged parameters are used to define the quantities

$$x_{e}(s) = \frac{\overline{k}_{e}(s) u(s)}{\beta_{e}(s)}$$
 (13)

and

$$\rho(s) = \frac{\beta(s)}{\beta_{c}(s)} . \tag{14}$$

which are used in turn to give the transmittance derivative function

$$y(s) = y[x_{e}(s), \rho(s)]$$
 (15)

The functional form of $y(x, \rho)$ with x and ρ depends on the line shape and the line strength distribution employed. The transmittance in the LS approximation is then given by Eq. (2) where \overline{W}/δ is given by

$$\frac{\overline{W}(s)}{\delta} = \int_{0}^{s} c(s') p(s') \overline{k}(s') y(s') ds' . \qquad (16)$$

A more detailed account of these approximations is given elsewhere. 1,5

⁵S. J. Young, <u>Band Model Formulation for Inhomogeneous Optical Paths.</u> TR-0075(5647)-4, The Aerospace Corp., El Segundo, Calif. (19 December 1974).

The important feature of both of these approximations is that the parameters \overline{k} , δ_e , and $\overline{\gamma}$ need to be known for the entire range of variation of the thermodynamic properties of the path. For the highly inhomogeneous optical path consisting of a long atmospheric slant path, plus a line-of-sight continuation through a hot-gas missile exhaust plume, for example, the path temperature T(s) can range from as low as $\sim 190\,^{\circ} \mathrm{K}$ to as high as $\sim 3000\,^{\circ} \mathrm{K}$. Thus, both \overline{k} and δ_e must be known for this same range of temperature variation in order to compute the path averages of Eqs. (10) and (11). It is this variation of \overline{k} and δ_e over large temperature ranges that is of primary concern. The variation of $\overline{\gamma}$ with temperature and pressure is adequately described by variations of the form $\overline{\gamma} \sim p/T^n$ where n is of the order of unity. Thus, $\overline{\gamma}$ will vary about an order of magnitude between the temperature limits indicated above. For this same temperature range, however, \overline{k} and δ_e may vary by several orders of magnitude.

B. BAND MODEL PARAMETERS FROM LINE DATA (LINAVE PARAMETERS)

If the line strength S(i) and line width $\gamma(i)$ of all the important lines in $\Delta \nu$ are known, the band model parameters \overline{k} , δ_e , and $\overline{\gamma}$ can be derived in terms of S(i) and $\gamma(i)$. The procedure is to force an exact agreement between the weak and strong limits of absorption for the statistical band model described in terms of the line parameters and the model described in terms of the band model parameters. For the former description, we write the mean equivalent width for all the lines in $\Delta \nu$ as

$$\frac{\overline{W}}{\delta} = \frac{1}{\delta} \left\{ \frac{1}{N} \sum_{i=1}^{N} W(i) \right\} = \frac{1}{\Delta \nu} \sum_{i=1}^{N} W(i)$$
 (17)

where W(i) is the equivalent width of the ith line. For a Lorentz line (and homogeneous path),

$$W(i) = 2\pi \gamma(i) L(x)$$
 (18)

where

$$\mathbf{x} = \frac{S(i) \, \mathbf{u}}{2\pi \, \gamma(i)} \quad . \tag{19}$$

The description in terms of band model parameters is given by Eqs. (1), (4), and (5). Repeating for convenience,

$$\frac{\overline{W}}{\delta} = \beta \ f(\mathbf{x}) \tag{20}$$

$$\beta = \frac{2\pi\overline{\gamma}}{\delta_{e}} \tag{21}$$

and

$$\mathbf{x} = \frac{\overline{\mathbf{k}}\mathbf{u}}{\mathbf{\beta}} \quad . \tag{22}$$

In the limit of weak absorption (that is, as $x \to 0$). Eqs. (17) through (19) give

$$\frac{\overline{W}}{\delta} \simeq \frac{u}{\Delta \nu} \sum_{i=1}^{N} S(i)$$

while Eqs. (20) through (22) yield

$$\frac{\overline{W}}{\delta} \simeq \overline{k}u$$
.

Equation of these two weak-limit expressions for \overline{W}/δ yields the solution for \overline{k}

$$\overline{k} = \frac{1}{\Delta \nu} \sum_{i=1}^{N} S(i) . \qquad (23)$$

For strong absorption (as $x \rightarrow \infty$), Eqs. (17) through (19), give

$$\frac{\overline{W}}{\delta} \simeq \frac{2\sqrt{u}}{\Delta \nu} \sum_{i=1}^{N} \sqrt{S(i) \gamma(i)}$$

while Eqs. (20) through (22) yield

$$\frac{\overline{W}}{\delta} \simeq 2 \sqrt{u} \sqrt{\frac{\overline{k} \overline{\gamma}}{\delta_{e}}} .$$

Equation of these two strong-limit forms for \overline{W}/δ yields the solution for $\delta_{\,{\bf e}}$

$$\frac{1}{\delta_{e}} = \frac{1}{k \gamma} \left[\frac{1}{\Delta \nu} \sum_{i=1}^{N} \sqrt{S(i) \gamma(i)} \right]^{2} . \tag{24}$$

The forced agreement for weak and strong absorption supplys two conditions for the determination of the three band model parameters. In order to complete the determination, we simply define $\overline{\gamma}$ to be

$$\overline{\gamma} = \frac{1}{N} \sum_{i=1}^{N} \gamma(i) \qquad (25)$$

Equations (23), (24), and (25) define the band model parameters \overline{k} , δ_e , and $\overline{\gamma}$ in terms of the line data S(i) and γ (i), i = 1,2, . . . , N.

These defining equations have been used to construct band model parameter sets for both $\rm H_2O$ and $\rm CO_2$. The line strength and width data were derived from the comprehensive line atlas compiled by AFCRL. This compilation provides line data for each of over 120,000 lines for seven atmospheric absorbing gas species including $\rm H_2O$ and $\rm CO_2$. The data given for each line include the line position ν (cm⁻¹), the line strength $\rm S_a$ (cm⁻¹/molecule-cm⁻² at 296°K), the line half-width $\rm Y_a$ (cm⁻¹ for air-broadening at 296°K and 1 atm pressure), and the energy of the lower level of the transition E (cm⁻¹). The line strength for the ith line at temperature T is computed from the value $\rm S_a$ given at the standard temperature $\rm T_a$ = 296°K by

$$S_{i}(T) = C(T) S_{a} \frac{Q_{R}(T_{a}) Q_{V}(T_{a})}{Q_{R}(T) Q_{V}(T)} \left[\frac{1 - e^{-\nu (i)/kT}}{1 - e^{-\nu (i)/kT}} \right]$$

$$\times \exp \left[-\frac{E(i)}{k} \left(\frac{1}{T} - \frac{1}{T_{a}} \right) \right] . \tag{26}$$

The factors Q_R and Q_V are the rotational and vibrational partition functions. respectively, of the molecule. The exponential term accounts for the

 $[^]st$ The compilation version dated 4 Feb 1975 by AFCRL was used in this work.

Boltzmann distribution population of molecules in the energy level E(i), and the term in brackets accounts for stimulated emission. The ratio of rotational partition functions is approximated by

$$\frac{Q_{R}(T_{a})}{Q_{R}(T)} \simeq \left(\frac{T_{a}}{T}\right)^{m} \tag{27}$$

where m = 1.5 for H_2O (H_2O is assumed to be a nearly symmetric-top molecule) and m = 1 for CO_2 . The molecular vibrational partition function is assumed to be the product of simple harmonic oscillator partition functions for each vibrational mode of the molecule:

$$Q_{V}(T) = \begin{bmatrix} -v_{1}/kT \end{bmatrix}^{-d_{1}} \begin{bmatrix} -v_{2}/kT \end{bmatrix}^{-d_{2}} \begin{bmatrix} -v_{3}/kT \end{bmatrix}^{-d_{3}}$$
(28)

where v_1 , v_2 , and v_3 are the fundamental oscillatory frequencies of the molecule and d_1 , d_2 , and d_3 are the degeneracies associated with these modes of vibration. For CO₂, $v_1 = 1388.17$ cm⁻¹, $v_2 = 667.40$ cm⁻¹, and $v_3 = 2349.16$ cm⁻¹. For H₂O, $v_1 = 3657.0$ cm⁻¹, $v_2 = 1594.7$ cm⁻¹, and $v_3 = 3755.7$ cm⁻¹. The degeneracies for all modes of both CO₂ and H₂O are unity, except for the doubly degenerate bending mode v_2 in the linear CO₂ molecule, for which $d_2 = 2$. The value of 1/k is 1.439 cm^{-°}K.

The factor C(T) of Eq. (26) converts the line strength from the AFCRL unit of cm⁻¹/molecule-cm⁻² to the unit cm⁻²/atm and is

$$C(T) = 2.480 \times 10^{19} \frac{296 \,^{\circ} \text{K}}{T} \frac{\text{molecules}}{\text{atm cm}^3}$$
 (29)

Equations (26) through (29) give the required line strengths S(i) to be used in Eq. (23) to calculate \overline{k} for any spectral interval $\Delta \nu$ and at any temperature T.

The line-broadening parameters of the AFCRL atlas are the broadening parameters appropriate to foreign gas broadening by air at 296°K. The mean line width parameter $\overline{\gamma}_a$ computed according to Eq. (25) will reflect broadening for these same conditions. Specification of the line-broadening parameter in terms of air broadening would be suitable if only atmospheric absorption paths were considered. In a hot, combustion gas environment, however, this description is not quite as appropriate. Now, account has to be made of broadening by H_2O and CO_2 as well. In addition, even if the concentrations of H_2O and CO_2 are small, the remaining gas is usually not air but N_2 (the O_2 having been used in the combustion process).

An adequate description of line pressure broadening for the species s is given by

$$\overline{Y}_{s}(p,T) = p \left[c_{s} \left(\overline{Y}_{s}^{*} \right)_{0} \left(\frac{273}{T} \right)^{n_{s}^{*}} + \sum_{f} \left\{ c_{f} \left(\overline{Y}_{s}^{f} \right)_{0} \left(\frac{273}{T} \right)^{n_{s}^{f}} \right\} \right] . \quad (30)$$

The summation term accounts for foreign gas broadening (f \neq s) and non-resonant self-broadening (f = s) contributions to the line width. The first term accounts for resonant self-broadening effects that occur primarily for H_2O . The c terms are the mole fractions of the gas constituents, and the $(\overline{\gamma})_0$ parameters are the broadening parameters for standard temperature (273°K) and pressure (1 atm) conditions. The exponents, n, determine the degree of temperature variation. Nominally, $n \sim 1/2$ and $n^* \sim 1$. Values of $(\overline{\gamma})_0$ and exponent parameters recommended in the NASA Handbook are given in Table 1.

Table 1. Line-Broadening Parameters for $\mathrm{H_2O}$ and $\mathrm{CO_2}^{\mathrm{a}}$

	n S	0.5	0.5	9	0.5	0.5	0.5	0.5	0.5
7	$(\frac{T}{Y_{\mathbf{S}}})_0$ (cm ⁻¹ /atm)	(60.0)	0.12	60.0	0.04	60.0	(0.07)	0.07	0.055
ນ	μ υ «	1.0	·		•	1.0			
	$(\frac{v}{v}_{s}^*)_0$ (cm ⁻¹ /atm)	0.44				0.01			
	Broadener (f)	H ₂ O	CO2	N 2	02	COS	H ₂ O	$^{\rm N}_{2}$	02
	Molecule (s)	н20				co ₂			

^aData taken from Rcf. 3. Values in parentheses are estimates.

Of the three parameters $(\overline{\gamma}_s)_0$, $(\overline{\gamma}_s)_0$, and $(\overline{\gamma}_s)_0$, the latter has been selected here as the fundamental line-broadening parameter; that is, the value for nonresonant self-broadening at STP. If $\overline{\gamma}_a$ is the mean width parameter for air broadening at 1 atm and 296°K computed according to Eq. (25), then Eq. (30) and Table 1 can be used to derive

$$\overline{\gamma}_0 \equiv (\overline{\gamma}_s^s)_0 = c \overline{\gamma}_a \tag{31}$$

where c=1.186 for $s=H_2O$ and c=1.405 for $s=CO_2$. The actual mean line width $\overline{\gamma}$ can be computed from the thermodynamic conditions of the optical path and $\overline{\gamma}_0$ by means of Eq. (30) written in the form

$$\overline{\gamma} = \overline{\gamma}_0 p \left[c_s \alpha_s^* \left(\frac{273}{T} \right)^{n_s^*} + \sum_f c_f \alpha_s^f \left(\frac{273}{T} \right)^{n_s^f} \right]$$
 (32)

where the α coefficients are the ratios of the $(\overline{\gamma})_0$ coefficients to $(\overline{\gamma}_s^s)_0$ and are obtained from Table 1 ($\alpha_s^s=1$). Note that none of these considerations on the line width parameters affect the evaluation of δ_e by Eq. (24) since any conversion factors applied to $\gamma(i)$ cancel.

For the present work, two sets of line-averaged band model parameters were generated. The set for H_2O (LINAVEH2O) contains \overline{k} (v, T), $1/\delta_e(v,T)$, and $\overline{\gamma}_0(v)$ for v=2500 to 4500 cm⁻¹ by steps of 25 cm⁻¹ with $\Delta v=25$ cm⁻¹ and for the 14 values of temperature T=100, 150, 200, 250, 300, 350, 400, 500, 750, 1000, 1500, 2000, 2500, and 3000°K. The set for CO_2 (LINAVECO2) contains the same parameters for the same temperatures but for v=3080 to 3860 cm⁻¹ by steps of 5 cm⁻¹ and $\Delta v=5$ cm⁻¹. In all cases, \overline{k} has the unit cm⁻¹/atm, δ_e has the unit cm⁻¹, and $\overline{\gamma}_0$ has the unit cm⁻¹/atm for nonresonant self-broadening at STP.

C. NASA PARAMETERS

Sets of band model parameters generated by General Dynamics and intended primarily for use in high-temperature combustion gas applications have been in existance for several years. The most recent publication of these parameter sets is given by Ludwig et al. in the NASA Handbook. 3

The data for CO_2 are the result of theoretical calculations based on the known quantum mechanical properties of linear triatomic molecules. The approach is similar to that presented in the preceeding section. Line strengths were computed theoretically and averaged to yield \overline{k} and δ_e . For the 2.7- μ m band region, \overline{k} values are given for the temperature range from 300 to 3000°K but δ_e is given only up to 1800°K. The δ_e data for temperatures between 1800 and 3000°K, however, can be obtained from the report by Huffaker and Dash. With the data from these two sources, a CO_2 band model parameter set (NASACO2) was constructed for ν = 3000 to 3770 cm⁻¹ by 5-cm⁻¹ steps and for the seven temperatures T = 300, 600, 1200, 1500, 1800, 2400, and 3000°K. The spectral resolution of the data appears to be

When required, linear interpolations with respect to ν and semilogarithmic interpolations with respect to T were used. The δ_e data at $\nu=3080$ cm⁻¹ was assumed to prevail between 3000 and 3080 cm⁻¹. The spurious temperature variation at T = 1200°K for 3110 $\leq \nu \leq$ 3150 cm⁻¹ was removed from the \overline{k} data by defining these values to be zero. An order-of-magnitude error in the 1200°K data at $\nu=3660$ cm⁻¹ was corrected in the \overline{k} data by using $\overline{k}=0.3471$ cm⁻¹ rather than the listed value of 0.03 ± 71 cm⁻¹. This correction also affects the values on either side of 3660 cm⁻¹; the \overline{k} value at 3655 cm⁻¹ was changed from 0.1877 to 0.3439 cm⁻¹ and the value at 3665 cm⁻¹ from 0.2197 to 0.3759 cm⁻¹. An apparent order-of-magnitude error in \overline{k} for T = 300°K at $\nu=3540$ cm⁻¹ was corrected by replacing the value 4.889 \times 10⁻² by 4.889 \times 10⁻³ cm⁻¹.

⁶W. Malkmus, <u>J. Opt. Soc. Am</u>. <u>54</u>, 751 (1964).

⁷R. M. Huffaker and M. J. Dash, <u>A General Program for the Calculation of Radiation from an Inhomogeneous</u>, <u>Noniosbaric</u>, <u>Nonisothermal Rocket Exhaust Plume</u>, NASA TM X-53622, <u>Marshall</u> pace Flight Center, Hunts-ville, Ala. (19 June 1967).

 $\Delta \nu \simeq 5 \text{ cm}^{-1}$. The NASA unit for \overline{k} is cm⁻¹ at STP and was converted to the unit cm⁻¹/atm by multiplication by 273/T. The $\overline{\gamma}_0$ coefficient is taken as a constant for all $\Delta \nu$ intervals with the value (from Table 1) $\overline{\gamma}_0 = 0.09 \text{ cm}^{-1}/\text{atm}$.

The NASA parameters for H2O were derived for the most part from experimental measurements. 8 Because of the nonlinearity of H2O, exact theoretical calculation of band model parameters is extremely complicated and difficult, particularly at high temperatures. The bulk of the H2O data above ~1200°K were obtained in a consistent manner from emission-absorption measurements made on very long strip-burner H2/O2 flames. Data below ~1200°K are based on extrapolations from these high-temperature data and on the analysis of published low-temperature $\rm H_2O$ spectra. For the 2.7- μm region, \overline{k} values are given for the temperature range from 300 to 3000°K. but δ_2 is given only down to 600° K. With these data, an H_2O band model parameter set (NASAH2O) was constructed between $\nu = 2500$ and 4500 cm⁻¹ by $25 - \text{cm}^{-1}$ steps at the seven temperatures T = 300, 600, 1000, 1500, 2000, 2500, and 3000°K. The spectral resolution of the data is $\Delta v = 25$ cm⁻¹. The 300°K values of δ_{α} at each wave number was obtained from a semilogarithmic extrapolation from the 600 and 1200°K data. Again, the unit of \overline{k} was converted from cm⁻¹ at STP to cm⁻¹/atm. and $\frac{1}{\gamma_0}$ was taken as (Table 1) $\frac{1}{\gamma_0}$ = 0.09 cm⁻¹/atm for all ν .

D. EVALUATION OF PARAMETER SETS

The AFCRL line atlas was compiled primarily for use in atmospheric transmittance problems. As a result, only those lines that are likely to be important near ambient atmospheric temperatures (say less than $\sim 300\,^{\circ}$ K) are specifically included. For most absorbing gases, these lines are absorption lines whose transition originates (in absorption) from the v=0 vibrational level of the ground electronic state of the molecule. For high-temperature problems, transitions originating from $v \ge 1$ (hot bands) are likely to be important. Although many lines for which $v \ge 1$ are included

⁸C. B. Ludwig, App. Opt. 10, 1057 (1971).

in the AFCRL atlas, it can be anticipated that the LINAVE band model parameters derived from the atlas data may not be adequate for temperatures much above 300°K.

Conversely, the NASA parameters were generated specifically for high-temperature applications. Here, the problem is that the parameters are not particularly useful for low-temperature problems. Indeed, neither the set for $\rm CO_2$ nor $\rm H_2O$ give any data for $\rm T < 300^{\circ}K$, the region of most importance for atmospheric application.

The deficiencies of both the LINAVE and NASA parameters have been investigated quantitatively by comparing absorption spectra computed through the use of the parameters with high-quality experimental measurements made for homogeneous paths. Comparisons were made for both CO₂ and H₂O and for both room-temperature and hot-gas conditions. The curve-of-growth function for the exponential-tailed inverse line strength distribution was used in the calculations.

1. CO₂ AT 296°K

Burch et al. ⁹ have made high-resolution measurements of the absorption spectra of CO_2 at 296°K for a wide variety of optical thickness, partial pressure of CO_2 , and total pressure (with N_2 as the foreign gas). For most of the sample experimental cases, extensive tables are given from which the integrated absorptance between any two wave numbers can be calculated. In Fig. 1, the solid curves are the $\overline{\tau}$ result for their sample no. 9 for which p=0.00763 atm, c=1.00, and L=237 m. The optical depth is u=181 atm cm. The curve was constructed for $\Delta v=5$ cm⁻¹ and extends through the band center region from 3450 to 3775 cm⁻¹. Figure 1(a) shows the comparison of the experimental spectrum with the spectrum computed with the

⁹D. E. Burch, D. A. Gryvnak, and R. R. Patty, <u>Absorption by CO₂ Betweer 3100 and 4100 cm⁻¹ (2.44-3.22 Microns)</u>, U-4132, Aeronutronic Div., Philco-Ford Corp., Newport Beach, Calif. (30 April 1968).

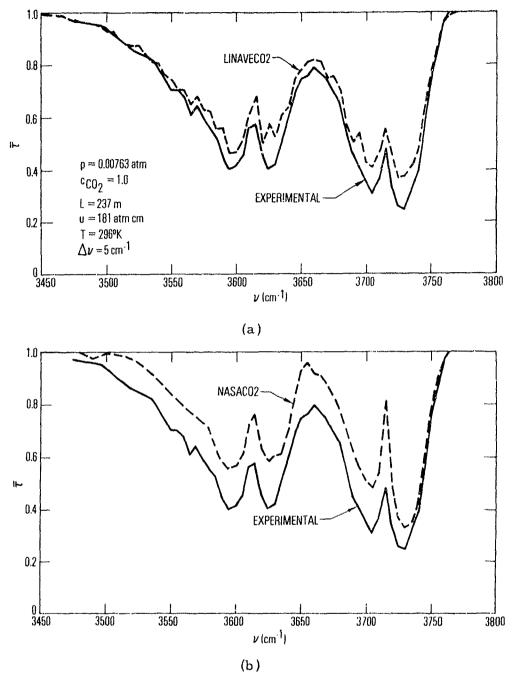


Fig. 1. Low-Temperature Transmission Spectra for CO₂ in the Band Center Region. The LINAVECO2 (a) and the NASACO2 (b) curves show spectra computed with the indicated band model parameter set. The EXPERIMENTAL curve is derived from the tables of Ref. 9 for sample no. 9 and for Δν = 5 cm⁻¹.

LINAVECO2 parameters while Fig. 1(b) shows the comparison with the result obtained with the NASACO2 parameters. Both of the parameter sets give results that underestimate the degree of absorption displayed by the experimental results. The LINAVECO2 set, though, gives results that are in adequate agreement with the experimental spectrum. The underestimation of the absorptance in both cases may be the result of using a statistical rather than a regular line-spacing band model for CO₂ at low temperatures.

A similar comparison was made in the far wing region between 3100 and 3500 cm⁻¹. Here, a much more strongly absorbing sample was chosen so that the absorptance would be measurable. The solid curves of Fig. 2 are the experimental results for sample no. 1 for which p = 2.5 atm, c = 1.00, and L = 933 m. The optical thickness is u = 2.33 \times 10⁵ atm cm and again, $\Delta \nu = 5$ cm⁻¹. The NASACO2 values for \overline{k} are zero at 300°K for $\nu \leq$ 3280 cm⁻¹ and consequently, no amount of absorption is effected in the band wing. The LINAVE parameters yield an absorption spectrum that is in adequate agreement with the experimental spectrum.

2. CO₂ AT 1200°K

A high-temperature emission comparison was made between calculated emissivity spectra and an experimental spectrum of Burch and Gryvnak.
The experimental conditions were: p = 0.997 atm, c = 1.00, L = 7.75 cm, and T = 1200 °K. The optical thickness is u = 7.73 atm cm and $\Delta \nu \simeq 7$ cm⁻¹. The comparison is shown in Fig. 3. Even at this high temperature, the result computed with the LINAVECO2 parameters is in good agreement with the experimental result above $\nu \simeq 3550$ cm⁻¹. In the wing region below 3500 cm⁻¹, however, the LINAVECO2 parameters seriously underestimate the degree of emission and, below 3450 cm⁻¹, predict no emission at all. The NASACO2

¹⁰ D. E. Burch and D. A. Gryvnak, Infrared Radiation Emitted by Hot Gases and Its Transmission Through Synthetic Atmospheres, U-1929, Aeronutronic Div., Philo-Ford Corp., Newport Beach, Calif. (31 October 1962).

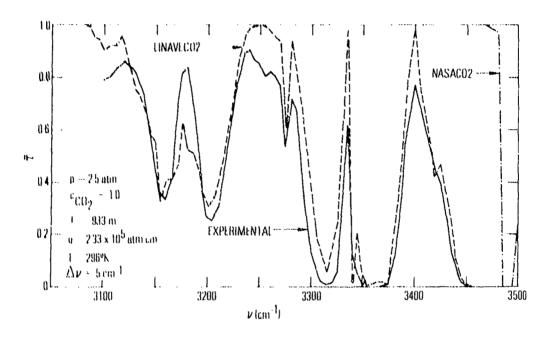
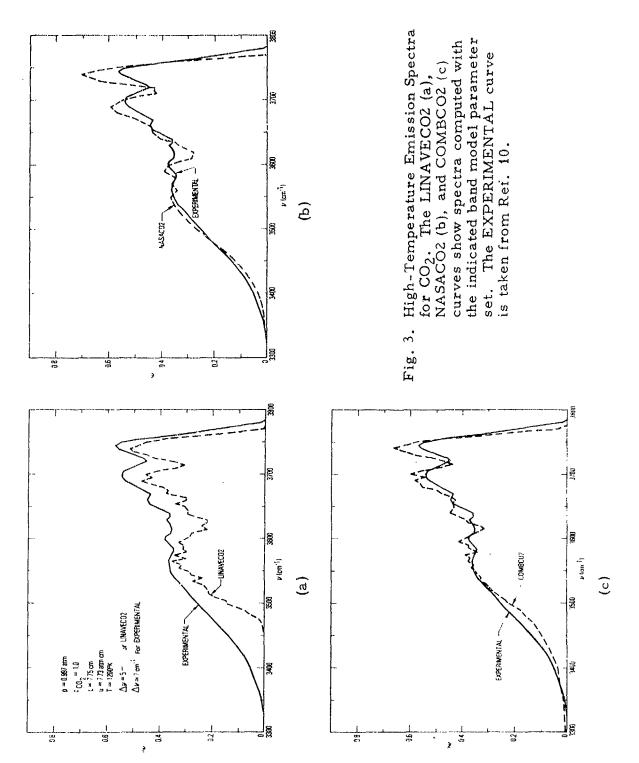


Fig. 2. Low-Temperature Transmission Spectra for CO₂ in the Band Wing Region. The LINAVECO2 and NASACO2 curves show spectra computed with the indicated band model parameter set. The EXPERIMENTAL curve is derived from the tables of Ref. 9 for sample no. 1 and for Δν = 5 cm⁻¹.



parameters, on the other hand, provide results that are in excellent agreement with the experimental spectrum for the whole spectral region below $v \approx 3600$ cm⁻¹ and that are in adequate agreement for the rest of the band.

3. H₂O At 296°K

High-resolution spectra and tables of integrated absorptance similar to those of CO_2 are given for H_2O by Burch et al. ¹¹ The solid curve of Fig. 4 is the transmittance spectrum for sample no. 39 with p = 0.951 atm, c = 0.0102 (with N_2 as the remaining gas), and L = 121 m. The optical thickness is u = 117 atm cm and $\Delta v = 25$ cm⁻¹. Figure 4(a) shows the comparison of the experimental spectrum with the spectrum computed with the LINAVEH2O parameters. The agreement between the two spectra is very good over the whole region from 2950 to 4300 cm⁻¹. Figure 4(b) displays the comparison with the result obtained using the NASAH2O parameters. As for CO_2 , only a general qualitative agreement exists between the two curves; the quantitative agreement is decidedly poor.

A comparison in the band center region from 3400 to 4200 cm⁻¹ for a less absorbing sample is given in Fig. 5. The experimental conditions (sample no. 38) are: p 0.176 atm, c = 0.031, L = 4.16 m, and u = 2.27 atm cm. Again, the LINAVEH2O parameters yield excellent agreement with experiment and the NASAH2O parameters, poor agreement.

A more strongly absorbing sample (sample no. 40) with p=0.20 atm, c=0.101, L=933 m, and u=1875 atm cm was used to show comparison in the wing region from 2800 to 3500 cm⁻¹. The results are given in Fig. 6 and again display the adequacy of the LINAVEH2O parameters and the inadequacy of the NASAH2O parameters at yielding accurate low-temperature H_2O absorption spectra.

¹¹D. E. Burch, D. A. Gryvnak, and R. R. Patty, Absorption by H₂O Between 2800 and 4500 cm⁻¹ (2.7 Micron Region), U-3202, Aeronutronic Div., Philco-Ford Corp., Newport Beach, Calif. (30 September 1965).

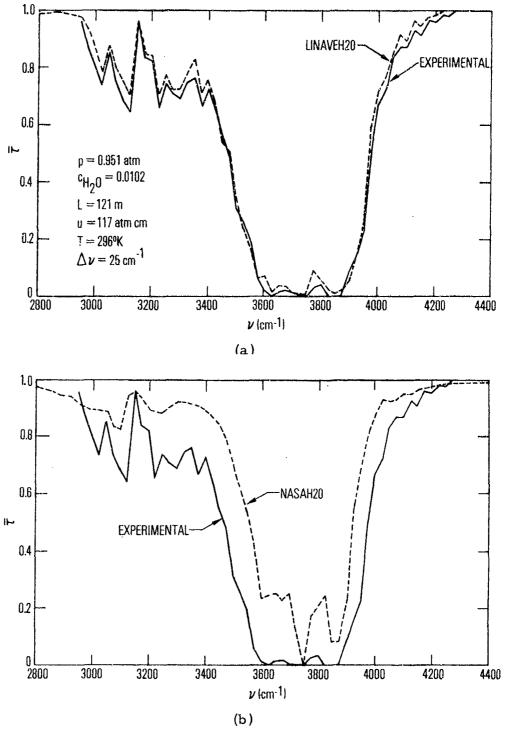


Fig. 4. Low-Temperature Transmission Spectra for H₂O. The LINAVEH2O (a) and NASAH2O (b) curves show spectra computed with the indicated band model parameter set. The EXPERIMENTAL curve is derived from the tables of Ref. 11 for sample no. 39 and for $\Delta v = 25$ cm⁻¹.

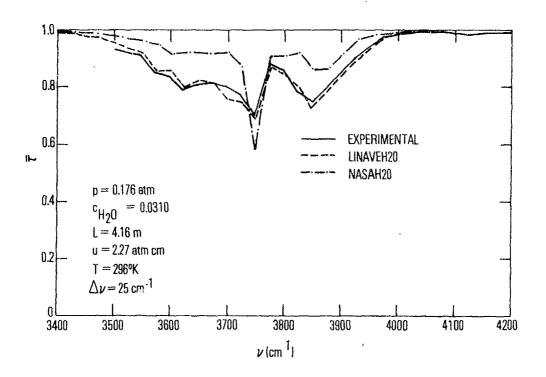


Fig. 5. Low-Temperature Transmission Spectra for H_2O in the Band Center Region. The LINAVEH2O and NASAH2O curves show spectra computed with the indicated band model parameter set. The EXPERIMENTAL curve is derived from the tables of Ref. 11 for sample no. 38 and for $\Delta v = 25$ cm⁻¹.

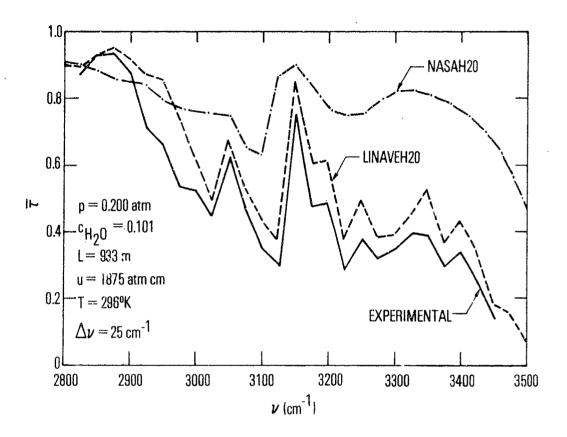


Fig. 6. Low-Temperature Transmission Spectra for H_2O in the Band Wing Region. The LINAVEH2O and NASAH2O curves show spectra computed with the indicated band model parameter set. The EXPERIMENTAL curve is derived from the tables of Ref. 11 for sample no. 40 and for $\Delta \nu = 25$ cm⁻¹.

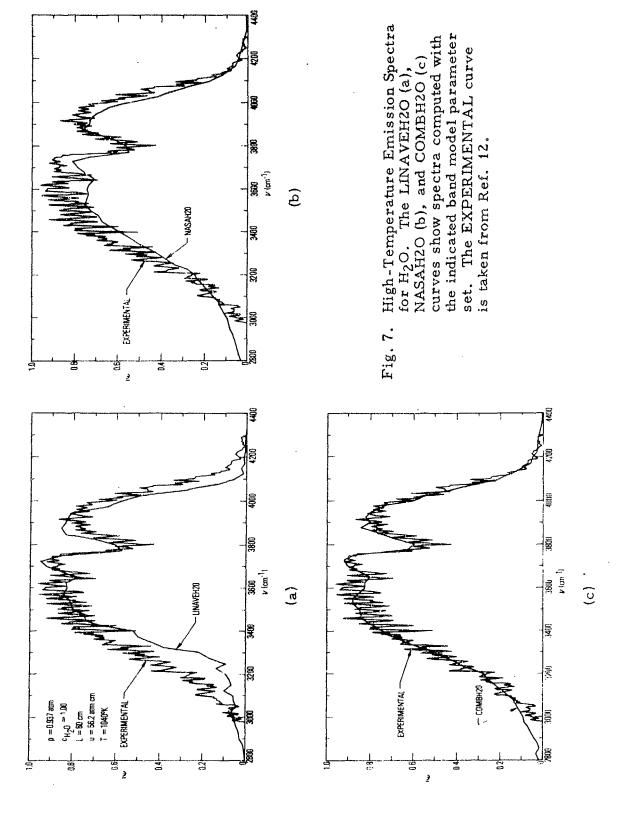
4. H₂O AT 1040°K

A medium resolution emissivity spectrum for pure H2O given by Simmons et al. 12 was used for this comparison. The experimental conditions are: p = 0.937 atm, c = 1.00, L = 60 cm, T = 1040°K, and u = 56.2 atm cm. The experimental spectrum and the results using the LINAVEH2O parameters are shown in Fig. 7(a) while the results using the NASAH2O parameters are shown in Fig. 7(b). In the band center region between 3400 and 4050 cm⁻¹, either set approximately reproduces the band contour of the experimental result, with the LINAVEH2O parameters possibly giving a slightly better fit. In the wing regions above 4050 cm⁻¹ and below 3400 cm⁻¹, the LINAVEH2O parameters significantly underestimate the emissivity. The NASAH2O parameters, on the other hand, provide results that are in excellent agreement with the experimental wing contours. There is a general underestimation of the emissivity by the NASAH2O parameters between 3400 and 3700 cm⁻¹. It should be remembered, however, that even at this temperature, these parameters are not experimentally measured but are extrapolated from higher temperature measurements. An example of the good fit between measured and computed values at 2500°K is given in Ref. 3.

These comparisons confirm the initial suspicions that the LINAVE parameters should be adequate for low-temperature applications but deficient at high temperatures whereas the converse is generally true for the NASA parameters. To summarize the comparison results:

- 1. The LINAVE parameters are adequate for both CO_2 and H_2O throughout the 2.7- μ m bands of these species for $T \simeq 300$ K.
- 2. The LINAVE parameters are adequate near the 2.7- μ m band centers for temperatures at least as high as T $\simeq 1000$ °K but are inadequate in the band wings for this and higher temperatures. This holds for both H₂O and CO₂.

¹² F. S. Simmons, C. B. Arnold, and D. H. Smith, Studies of Infrared Radiative Transfer in Hot Gases, I: Spectral Absorptance Measurements in the 2.7μ H₂O Bands, Rep. No. 4613-91-T, Willow Run Laboratory, Ann Arbor, Mich. (August 1965).



- 3. The NASA parameters are adequate for both CO₂ and H₂O throughout the 2.7- μ m bands of these species for temperatures above T \simeq 1000 °K.
- 4. The NASA parameters are inadequate for both H_2O and CO_2 anywhere in the 2.7- μ m spectral region for $T \approx 300$ °K.

III. COMBINED PARAMETER SETS

A. GENERAL PROCEDURE

Parameter sets for both CO₂ and H₂O that are consistent for the whole temperature range from 100 to 3000°K were generated by combining the low-temperature variation of the LINAVE parameters with the high-temperature variation of the NASA parameters. This combination was performed at each spectral position by making semilogarithmic plots of the parameters from each set as functions of temperature, and connecting some "low" temperature point on the LINAVE curve with some "high" temperature point on the NASA curve. The designations "low" and "high" temperature are relative terms only, since the connection at some spectral positions was best done by connecting, for example, the 1000°K value for the LINAVE parameter with the 1500°K value for the NASA parameter or, in other cases, the 250°K value of the LINAVE parameter with the 300°K value for the NASA parameter. Examples of the method are given in Figs. 8 through 11 for several spectral intervals for both CO₂ and H₂O.

This procedure is admittedly subjective, although several rules and guidelines were followed for making the transition from one curve to the other:

- 1. The transition from one curve to the other should make the overall variation as smooth as possible.
- 2. The LINAVE parameters for T ≤ 300 °K should remain reasonably unchanged.
- 3. The NASA parameters for $T \gtrsim 2000$ K should remain reasonably unchanged.
- 4. No redefinition of parameter values in either set is made. The temperature variation of the combined set consists of established values from one set or the other, or values interpolated from the transition line.
- 5. The match-up for each spectral interval should be consistent with the match-up made for adjacent spectral intervals.
- 6. The match-up for δ_e should reflect a monotonic increase of the density $(1/\delta_e)$ with temperature.

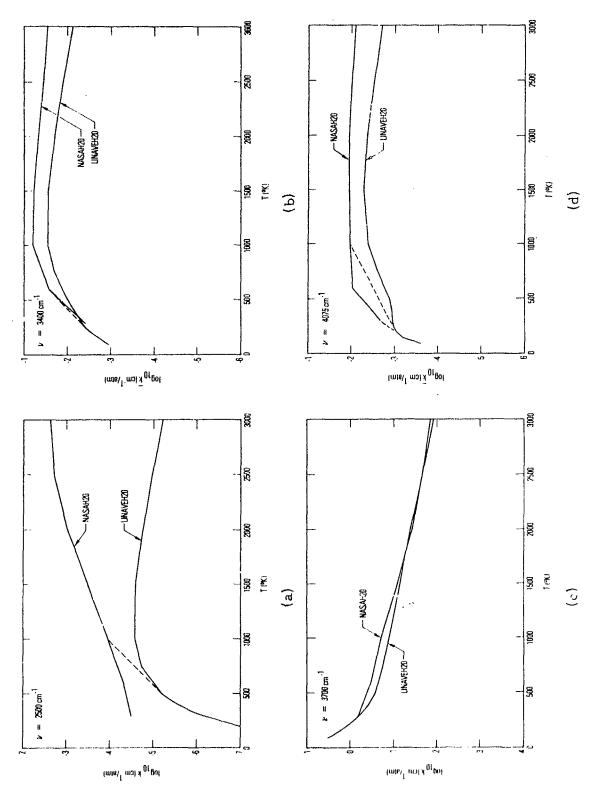
Even with these guidelines, several ways of connecting the sets were sometimes possible. An iterative procedure was used in these cases. A first-guess match-up was made and spectra generated for the homogeneous path conditions described in the previous section. A comparison of these spectra with the experimental curves and inspection of the parameter plots were made to see if another transition line would give a better result. If it could, the change was made and tested by generating new spectra for comparison.

B. H₂O PARAMETER SET (COMBH₂O)

Parameter plots for both \overline{k} and $1/\delta_e$ were made for 81 spectral positions from 2500 to 4500 cm⁻¹ (equal steps of 25 cm⁻¹). The four main types of variations for \overline{k} that occurred are shown in Fig. 8. The LINAVEH2O variation displayed in Fig. 8(a) ($v=2500~{\rm cm}^{-1}$) is typical for all of the spectral intervals in the band wing region. The absorption coefficient increases with temperature up to $\sim 1000~{\rm K}$ but thereafter levels off or falls slightly. The increasing discrepancy between the LINAVEH2O and the NASAH2O curves reflects the lack of hot band lines in the AFCRL atlas for the wing region.

Figures 8(a) (ν = 2500 cm⁻¹) and 8(d) (ν = 4075 cm⁻¹) show variations in which several reasonable transition lines could be drawn. In the latter (ν = 4075 cm⁻¹), the line from 150°K on the LINAVEH2O curve to 300°K on the NASAH2O curve was the first guess based on the "smoothness" criterion. Better overall agreement with the experimental spectra, however, was obtained using the transition line from 300°K on the LINAVEH2O curve to 1000°K on the NASAH2O curve. The variations at ν = 3400 and 3700 cm⁻¹ [Figs. 8(b) and 8(c), respectively] are examples where little judgment was required to make the match-up. In general, throughout regions of strong absorption, the match-up procedure was relatively self-evident.

The variations of δ_e for H_2O with temperature were very consistent throughout the whole spectral region and were simple variations of the forms shown in Fig. 9. In all cases, the first-guess match-up was sufficient.



是一个人,也是一个人,也是一个人,他们也是一个人,他们也是一个人,他们也是一个人,他们也是一个人,也是一个人,也是一个人,也是一个人,他们也是一个人,他们也是一

LINAVEH2O and NASA112O curves are the variations for the indicated band model parameter set; dushed curves show transitions from one curve to Variation of K(H2O) with Temperature for Selected Spectral Intervals. the other. ∞• Fig.

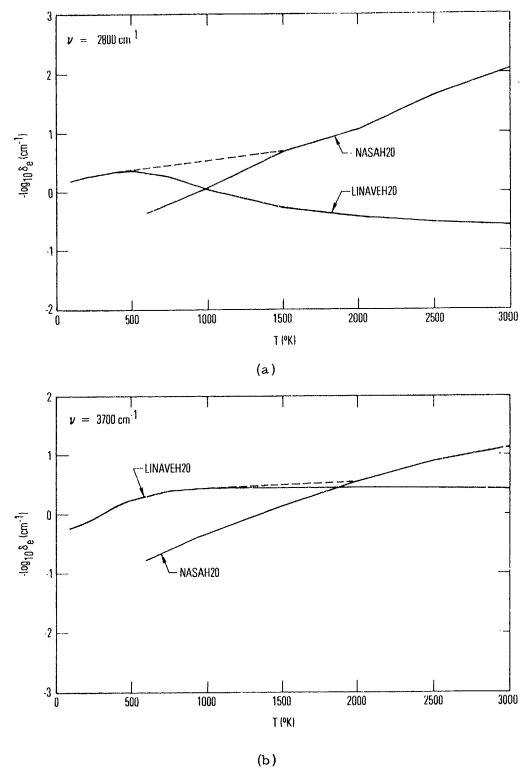


Fig. 9. Variation of $1/\delta_e$ (H₂O) with Temperature for Selected Spectral Intervals. The LINAVEH2O and NASAH2O curves are the variations for the indicated band model parameter set; dashed curves show transitions from one curve to the other.

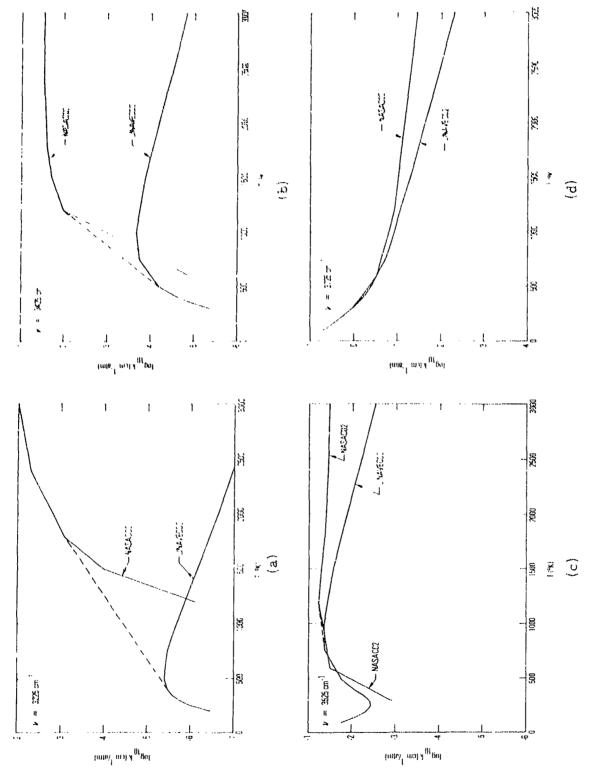
A final parameter set was generated for $\rm H_2O$ for the spectral region $\nu=2500$ to $4500~\rm cm^{-1}$ by steps of 25 cm⁻¹ and reflects a spectral resolution of $\Delta\nu=25~\rm cm^{-1}$. The tertemperature values T = 100, 200, 300, 500, 750, 1000, 1500, 2000, 2500, and 3000°K were chosen to represent the temperature variation. The mean line width parameter $\overline{\gamma}_0$ from the LINAVEH2O set was chosen to represent this parameter for the combined set. Spectra for the homogeneous path conditions of Sect. II were generated with the final parameter set to verify its validity. For all of the low-temperature cases, the spectra generated with the COMBH2O parameters were indistinguishable (in plots) from those generated using the LINAVEH2O parameters. The spectrum for the 1040°K path is shown in Fig. 7(c). The overall agreement with the experimental curve is better than was obtained with either the LINAVEH2O or NASAH2O parameters. A tabulation of the COMBH2O parameter set is included in the Appendix.

C. CO₂ PARAMETER SET (COMBCO₂)

Parameter plots for \overline{k} and $1/\delta_e$ were made for the 135 spectral positions from 3100 to 3770 cm⁻¹ (equal steps of 5 cm⁻¹). Examples of match-ups are illustrated in Fig. 10. In the band wing region, the variation of the LINAVE \overline{k} parameter is similar to that for H_2O in the wing region. That is, the value increases with temperature up to about 500°K and then decreases owing to the lack of data in the AFCRL compilation for hot band lines. The examples for $\nu = 3525$ and 3725 cm⁻¹ in Fig. 10 are cases where the match-up is easily made.

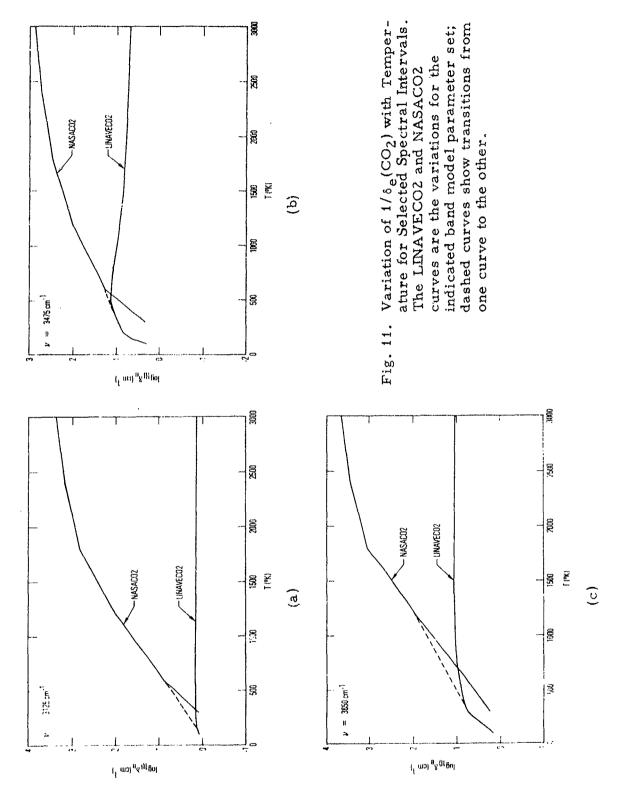
Examples of the match-up of the line spacing parameter $\delta_{\rm e}$ are shown in Fig. 11. In most cases, the selection of the transition line was reasonably self-evident.

After several match-up iterations, a final parameter set was generated for CO_2 for the spectral region $\nu=3100$ to 3770 cm⁻¹ by steps of 5 cm⁻¹ and reflects a spectral resolution of $\Delta\nu=5$ cm⁻¹. The same ten temperatures as for H_2O were chosen to represent the temperature variation of the set.



報酬を経過性に対象を表現している。 は、1987年 1987年 1

Variation of $\overline{k}(CO_2)$ with Temperature for Sclected Spectral Intervals. The LINAVECO2 and NASACO2 curves are the variations for the indicated band model parameter set; dashed curves show transitions from one curve to the other. Fig. 10.



このかかち、このことのなるから、からしているのはないながられるとなるないのでは、

The mean line width parameter γ_0 from the LINAVECO2 set was chosen to represent this parameter in the final set. The k and $1/\delta_e$ parameters of the LINAVECO2 set are zero for the 5-cm⁻¹ intervals centered on ν = 3245 and 3250 cm⁻¹ because no lines occur in these regions. The data from the NASACO2 set for the whole temperature range were used for these intervals.

Spectra for the homogeneous path conditions of Sect. II were computed with the final parameter set to verify its validity. For the low-temperature cases, the results were indistinguishable from the LINAVECO2 curves of Figs. 1 and 2 except in the 3625- and 3725-cm⁻¹ valleys, where a slight improvement in agreement with the experimental curve was noted. The spectrum for the 1200°K case is shown in Fig. 3(c). The overall agreement with the experimental curve is better than was obtained with either the LINAVECO2 or NASACO2 parameters. A tabulation of the COMBCO2 parameters is included in the Appendix.

IV. ATMOSPHERIC TRANSMITTANCE CALCULATION

In Ref. 1, radiative transfer calculations for two atmospheric paths and a hypothetical hot H_2O/CO_2 plume at 20-km altitude were made with either the LINAVE or NASA parameters. The results for the slant path (20 km to space at a 75-deg zenith angle) have been recomputed for the LINAVE and NASA parameters and are compared here with the results obtained using the COMB parameters. The source path represents a single line of sight through the diameter position of a homogeneous, isothermal, circular cylindrical plume at an aspect angle of 90 deg. The source path length is 7.73 m, the temperature is 1249°K, the mole fraction of H_2O is 0.2533, and the mole fraction of H_2O is 0.2533, and the mole fraction of H_2O is 0.2533. The calculations were performed for the Lorentz line shape, with an exponential-tailed inverse line strength distribution, and used the Lindquist-Simmons approximation.

The band model parameters for CO_2 were reduced in resolution from 5 to 25 cm⁻¹ in order to be compatible with the resolution of the H_2O parameters. The band model parameters for the 5-cm⁻¹-wide interval centered on ν_i and the parameters for the two lower and two higher adjacent intervals were averaged to give the parameters for the 25-cm⁻¹-wide interval centered on ν_i according to

$$\overline{k} = \frac{1}{5} \sum_{j=i-2}^{i+2} \overline{k}(j)$$

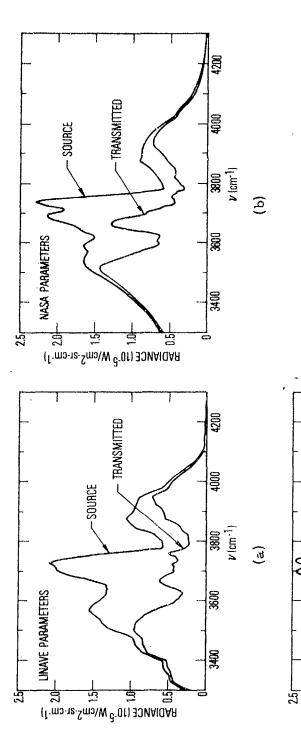
¹³R. A. McClatchey, R. W. Fenn, J. E. A. Selby, F. E. Volz, and J. S. Garing, Optical Properties of the Atmosphere (Revised), AFCRL-71-0279, Air Force Cambridge Research Laboratories, Mass. (10 May 1971).

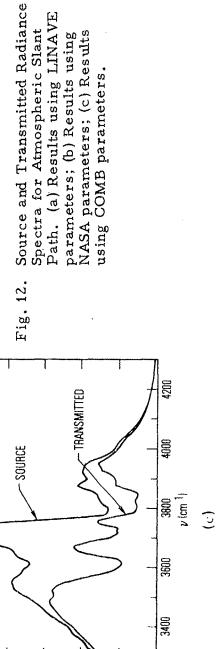
$$\overline{\gamma}_0 = \frac{1}{5} \sum_{j=i-2}^{i+2} \overline{\gamma}_0$$
 (j)

and

$$\frac{1}{\delta_{e}} = \frac{1}{\overline{k} \overline{\gamma}_{0}} \left[\frac{1}{5} \sum_{j=2}^{i+2} \sqrt{\frac{\overline{k} (j) \overline{\gamma}_{0} (j)}{\delta_{e} (j)}} \right]^{2}$$

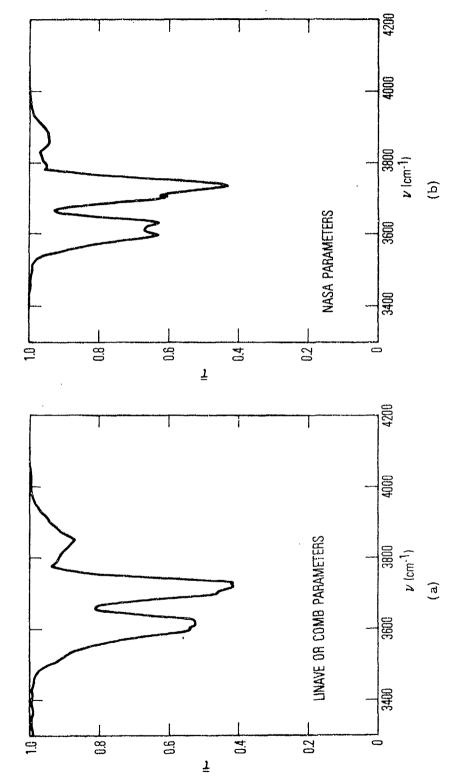
The results obtained with the three parameter sets for the radiance at the boundary of the source and after transmission along the absorbing atmospheric path re shown in Fig. 12. The transmittance τ , obtained without account of line correlation, is illustrated in Fig. 13. Similarly, the effective transmittance of the atmosphere $\overline{\tau}_{o}$, obtained by taking account of line correlation between the source emission spectrum and the atmospheric absorption spectrum, is given in Fig. 14. Detailed discussions of the source radiance and atmospheric transmittance $\overline{\tau}$ spectra are not required since these would parallel those already given in Sect. II of this report. The only new result displayed by these spectra is the effective transmittance $\bar{\tau}_{a}$ (Fig. 14). Although T is a source-dependent quantity and, therefore, depends on the band model parameters used to describe the source emission, there is a great similarity between the $\overline{\tau}_e$ spectra computed using the LINAVE and COMB parameters. A comparison between the NASA and COMB results, on the other hand, reveals a significant dissimilarity. These results would indicate that an accurate description of the atmosphere (that is, an accurate knowledge of band model parameters for low temperatures) is more important than an accurate description of the hot gas source in determining $\overline{\tau}_{ij}$.





COMB PARAMETERS

ARDIANCE (110.⁵ W/cm²-sr-cm-1)



Transmittance Spectra for Atmospheric Slant Path. (a) Results using LINAVE or COMB parameters; (b) Results using NASA parameters. Fig. 13.

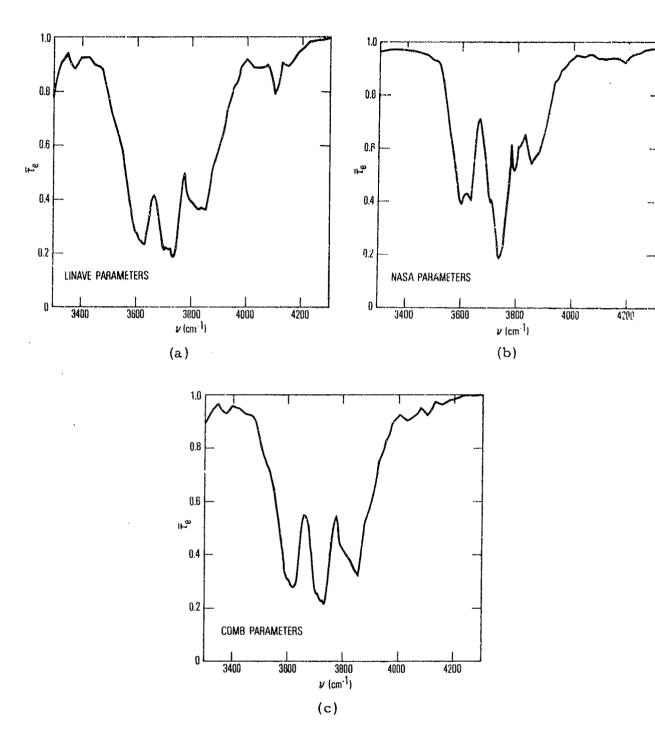


Fig. 14. Effective Transmittance Spectra for Atmospheric Slant Path.
(a) Results using LINAVE parameters; (b) Results using NASA parameters; (c) Results using COMB parameters.

APPENDIX

COMBH2O AND COMBCO2 PARAMETER SET LISTINGS

Tabulations of the COMBH2O and COMBCO2 parameters are given in Tables A1 and A2, respectively. A description of these listings follows. IDNAME is simply an identification name for the parameter set. RESOLUTION is the value of $\Delta \nu$ appropriate for the set. ALPHA (1) through ALPHA (5) are the ratios of the efficiency of pressure broadening by the indicated mechanisms to that of nonresonant self-broadening. ALPHA (6) is the atomic mass of the absorbing species. The WAVENUMBER array lists the center value of all the Δv intervals included in the set. NW is the number of such intervals. The TEMPERATURE array similarly lists the temperatures for which the data are tabulated. NT is the number of such temperatures. The ABSORPTION COEFFICIENT array is k. The first column of this array is the interval center wave number, and the rows are the values at the temperatures of the TEMPERATURE array. The EFFECTIVE LINE DENSITY array is the parameter $1/\delta_{\underline{e}}$ and is presented in the same format as $\overline{k}.$ The MEAN LINE WIDTH array is the parameter $\overline{\gamma}_0$ for nonresonant self-broadening at STP. The values correspond to the wave numbers listed in the WAVENUMBER array.

Set
Parameter
Model
Band N
COMBH20 B
of (
Listing
e A1.
Tabl

A P A 2 2 2 2 2 2 2 2 2	PPHAR (S)	390E+0	25.0000
Park # 3 Park	5000 2000 2000 2000	338F40	PESONANT SELF-BROADENING
N		0000 0000 0000 0000 0000 0000 0000 0000 0000	OFEIGN-SAS BROADENINGTON OFEIGN-GAS BROADENINGTOO OFEIGN-GAS BROADENINGTOOS
2.556.613 2.5556.613 2.5550.6143 2.6550.61	MAVENUMBERCHI	APR	1) NH
\$2500E+03 3.2075E+03 3.0500E+03 3.3076E+03 3.1076E+03 3	00E+03 2 50E+03 2	525E+0 775E+0	.550E+03 2.575E+03 2.600E+03 2.625E+03 2.650E+03 2.675E+03 2.700E+03 2.705E+0 .800E+03 2.825E+03 2.850E+03 2.875E+03 2.630E+03 2.675E+103 2.705E+03 2.705E+0
E-808E+83 4.255E+83 4.050E+83 4.105E+83 4.106E+83 4.155E+83 4.156E+83 4.156E	10000000000000000000000000000000000000	025E+8 275E+8 525E+0 775E+0	*050E+03 3.075E+03 3.100E+03 3.125E+03 3.150E+03 3.150E+03 3.175E+03 3 3.050E+03 3.255E+03 3.375E+03 3.050E+03 3.055E+03 3.05E+03
ENSERATURE(T) ARRAY(DEGK) NT= 10 BSJRPTION COEFFICIENT(K) ARRAY(CM-1/ATY) BSJRPTION COEFFICIENT(K) BSJRPTION CO		275E+0	•858E+03 4.075E+03 4.100E+03 4.325E+03 4.420E+03 4.425E+03 4.425E+03 4.450E+03 4.455E+0 •300E+03 4.325E+03 4.350E+03 4.375E+03 4.420E+03 4.425E+03 4.455E+03 4.455E+03 4.455E+03 4.455E+03 4.455E+0
853RPTION COEFFICIENT(K) ARRAY(CM-1/ATY) 853RPTION COEFFICIENT(K) ARRAY(CM-1/ATY) 863RPTION COEFFICIENT(K) 863RPTION COEFFICIEN	EMJERATURE() ARRAY (X) NT= 1
851RPTION COEFFICIENT(K) ARRAY(CM-1/ATY) 89.180F-09 3.109E-07 6.922E-07 5.952E-05 2.655E-05 1.026E-04 3.059E-04 9.132E- 80.3.5.36E-03 3.548E-07 3.4014E-05 7.062E-05 1.026E-04 3.059E-04 9.132E- 80.3.5.36E-03 3.548E-07 3.4014E-05 7.062E-05 1.026E-04 3.039E-04 8.885E- 80.3.5.36E-07 3.588E-07 3.4014E-05 7.062E-05 1.013E-04 3.039E-04 8.885E-00 1.641E-05 7.875E-05 1.013E-04 3.039E-04 8.954E-00 1.641E-05 7.875E-05 1.013E-05 1.013E-04 3.039E-04 9.185E-00 1.641E-05 7.875E-05 1.013E-04 3.039E-04 9.185E-00 1.641E-05 7.875E-05 1.013E-05 1.013E-04 3.039E-04 1.389E-04 1.389E-04 1.576E-05 1.013E-05 1.013E-04 1.389E-04 1.576E-04 1.576E-05 1.048E-04 1.576E-04 1.765E-04 1.576E-04 1.376E-04 1	.808E+02 2	000E+0	.000E+02 5.000E+02 7.500E+02 1.000E+03 1.500E+03 2.000E+03 2
0 9.160E-09 1.109E-07 6.922E-07 5.952E-06 3.183E-05 1.026E-04 3.058E-04 9.132E-09 3.538E-03 3.548E-07 3.4109E-07 7.0652E-06 3.183E-05 1.026E-04 3.039E-04 8.352E-09 3.548E-07 3.4109E-07 3.410E-06 3.183E-05 1.026E-04 3.039E-04 8.352E-00 3.541E-05 1.624E-07 3.039E-04 8.352E-00 3.541E-05 3.651E-05 3.039E-04 3.039E-04 8.352E-00 3.551E-05 3.651E-05 3.039E-04 3.353E-04 3.039E-04 3.039E-04 3.039E-04 3.039E-04 3.353E-04 3	BSJRPTION C	EFFICIE	(K) ARRAY(CM-1/AT
00 2.515E-05 1.524E-05 2.350E-05 3.558E-05 7.008E-05 1.013E-04 3.034E-04 9.185E-05 1.641E-05 7.375F-05 4.231E-05 7.558E-05 1.013E-04 3.034E-04 3.185E-05 1.485E-05 7.375F-05 7.375F-05 1.008E-04 3.034E-04 3.185E-04 1.375F-05 7.375F-05 1.485E-04 3.036E-04 1.375F-05 7.375F-05 1.485E-04 1.375F-04 1.375E-04 1.3	00 9.160E-0	45.00 A 45.00	7 6.922E-07 5.952E-06 2.471E-05 1.026E-04 3.058E-04 9.132E-04 1.813E-03 2.257E- 7 1.824E-06 7.062E-06 2.656E-05 9.992E-05 3.039E-04 8.885E-04 1.704E-03 2.256E- 7 3.400E-06 9.872E-06 3.183E-05 1.026E-04 3.039E-04 3.750E-04 1.550E-03 2.284E-
80 2-042E-04 9-852E-05 9-191E-05 8-823E-05 1-201E-04 2-078E-04 5-897E-04 1-447E- 80 3-322E-04 1-541E-04 1-338E-04 1-270E-04 1-595E-04 2-435E-04 3-026E-04 1-746E-04 3-322E-04 3-026E-04 1-746E-04 1-746E-04 1-746E-04 1-746E-04 1-746E-04 1-746E-04 1-746E-04 1-759E-04 1-746E-04 1-	00 2.516E-0 00 1.641E-0 00 7.411E-0	1.624E 3.875F 7.368F	5 2.350E-05 3.568E-05 6.012E-05 1.013E-04 3.094E-04 9.185E-5 4.231E-05 5.042E-05 7.008E-05 1.048E-0+ 3.258E-04 1.389E-5 5.752E-05 5.150E-05 7.926E-05 1.3088E-0+ 3.558E-04 1.375E-5 5.857E-05 7.877E-05 9.695E-05 1.485F-04 4.537E-04 1.375E-0
00 2.065E-04 1.376E-04 1.208E-04 1.879E-04 3.187E-04 5.378E-04 1.372E-03 2.525E-00 1.050E-04 1.372E-03 2.798E-00 1.050E-04 1.017E-03 2.798E-00 1.050E-04 1.017E-03 2.798E-00 2.877E-05 1.017E-05 2.798E-00 2.877E-05 4.817E-05 4.911E-03 2.79E-05 1.107F-04 2.705E-04 1.616E-03 3.194E-00 2.487E-05 2.599E-05 3.194E-05 2.487E-05 2.599E-05 3.275E-05 3.194E-05 2.487E-05 2.599E-05 3.275E-05 3.194E-05 2.487E-05 2.595E-05 3.194E-05 3.19	30 2.042E-0	9.65 9.65 9.65 9.65 9.65 9.65 9.65 9.65	5 9.191E-05 8.823E-05 1.201E-04 2.076E-04 5.897E-04 1.447E-03 2.523E-03 2.684E- 4 1.338E-04 1.270E-04 1.595E-04 2.435E-04 3.026E-04 1.706E-03 2.806E-03 2.894E- 4 1.776E-04 1.574E-04 1.864E-04 2.730E-04 9.082E-04 2.008ZE-04 3.221E-03 3.221E-0 6 2.375E-04 2.574E-04 2.545E-04 3.425E-04 3.425E-03 3.221E-03 3.425E-03 3.405E-03 3.405E-03 3.405E-03 3.405E-03 3.405E-03 3.405E-03 3.405E-03 3.405E-04 3.
THE PARTY OF THE PROPERTY OF THE PARTY OF TH	00 2.065E-000 1.050E-000 5.877E-0	1.376E 1.017E 4.817E	4 1.20%E-04 1.879E-04 3.167E-04 5.327E-04 1.372E-03 2.525E-03 3.964E-03 3.795E- 4 1.325E-04 2.252E-04 3.948E-04 6.470E-04 1.511E-03 2.798E-03 4.073E-03 4.177E- 5 4.90FE-05 6.139E-05 1.107E-04 2.705E-04 1.616E-03 3.194E-03 4.77E-03 4.550E- 5 3.565E-05 8.059E-05 1.766F-04 3.950E-04 0.005E-03 3.75E-03 4.055E-03 6.50EE
00 1.5045F=100 0.41401F=100 0.6045F=100 5.5045F=104 4.4447F=104 7.5047F=104 5.5045F=105 5.505F=106 7.5045F=107 4.7244F=107 0.577F=106 7.5045F=107 4.7244F=107 0.5045F=107 4.7244F=107 0.5045F=107 0.577F=107 0.5045F=107 0.504	00 1.344E-0	3.181E	5 6.802E-05 2.349E-64 4.442E-04 7.677E-04 2.293E-03 3.986E-03 5.788E-03 5.478E-5 1.798E-03 5.478E-

	ł
mamanananananananananananananananananan	saaaaaa saaaaaa
	F F F F F
The way of the second and the second	Jac Colin Co
ショル・ドランカ ロカラロ 自己さん にゅす アンスタン とうしゅう インスター インス マッシュ タッシュ インス とり インス・フィント アンス・フィント かんしょう インス・フィント アンス・フィント アンス・フィント アンス・フィント アンス・フィント アンス・フィント アンス・アンス・アンス・アンス・アンス・アンス・アンス・アンス・アンス・アンス・	340m40
OF SIR DUM HELD AND CONTROL OF THE SIR DUM HELD CONTROL OF THE SIR DUM HE SIR DUM HELD CONTROL OF THE SIR DUM HE SIR DUM HE SIR DUM HE SIR DUM	। १० सम्बन्ध
de d	
ស្រីស្រីស្រីស្រីស្រីស្រីស្រីស្រីស្រីស្រី	பயய்யய்
$\frac{\partial \mathcal{V}}{\partial \mathcal{V}} = 0 + 44 + 44 + 44 + 44 + 44 + 44 + 44 $	- OPENIMO - HIVOIDO
MADONION TO BOUND BOUND TO THE MANAGEMENT OF THE AND TO SHE THE THE TOP TO SHE THE THE TOP TO SHE THE THE THE THE THE THE THE THE THE T	ひている
้อน สู่อ คำคำคำคำผู้เกิดเกาะ หาย เกาะ หาย เกาะ เกาะ สุดิตตาม และ สุดิตตาม เกาะ สุดิตตาม เกาะ สุดิตตาม เกาะ สุดิตตาม	and visited to
4 m mm no analy and analy and analy and analy and analy and	tttmm
mamanandanandanandanandanandandandandandand	
ការក្រសារក្រសារក្សាស្ត្រ ក្រសារក្រសារក្រសារក្សាសាក្សាស្ត្រាសាក្សាសាក្សាសាក្សាសាក្សាសាក្សាសាក្សាសាក្សាសាក្សាសាក	
TO A THE TOWN WANT OF THE TOWN WE WAS TO THE TOWN WANT OF	1 COCHE
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
томертного и пометь применти и пометь в пометь и пометь пометь пометь пометь пометь пометь пометь пометь пометь	444-0000

	1 1 1 1 1
よりこく 4000 エーディングをついっしょう アン・エー・エー・エン・エン・エン・エン・エン・エン・エン・エン・エン・エン・エン・エン・エン・	- LONDON
Person les controls de la colonidad de la colo	42000 4.4

	် ဝင်ဝင်ခ
រង្គរង្គរង្គរង្គរង្គរង់រង់រង់រង់រង់រង់ ជាមួយជាង ជាមួយជាង ប្រជាជាង ប្រជាជាង ជាមួយជាង ស្រាប់ ជាប្រជាជាង ស្រាប់ ជាប្រ	บเมนเมนามัน
THE	ാഹസ വയും വെഡ് ഡസ യം
Manual des actions and the property of the pro	
THE COMMAND AND AND AND AND AND AND AND AND AND	No a superior
	300000
பிய வக்கியம் வகியம் வெய்ய வக்கிய வக்க	1000-
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2002000
OH HE WIND WHEN THE WAS A SHOWN TO SHOW THE WAS A SHOWN THE WAS A SHOW	77.04.0
an an un	
	the state of the state of
TO ME TO THE WIND THE WASHINGTON TO THE WASHINGTON THE WASHINGTON THE WASHINGTON TO THE WASHINGTON TO THE WASHINGTON TO THE WASHINGTON TO	
The state of the s	၁ သက္ကရာ အဆ
the many winding and the many	4-10-K-01-41
43 MM MM MANAMAMAMAMAMAMAMAMAMAMAMAMAMAMAM	
	- N & WASIN
PP 40 80 W DO SUNDON TOWN WOUND AND AND AND AND AND AND AND AND AND A	JA HIMNA
THE TANK TO	• • • •
$\frac{1}{1} \frac{1}{1} \frac{1}$	200000 70 4000
11 11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	լ լ լ լ լ լ լ լ լ
日まれてするのであるは、000人もできるものものではましてのからくものできるののできた。4人とは、10人は10人は10人は10人は10人は10人は10人は10人は10人は10人は	N-10100
- App はこうような (大力) とうしょうしょう しゅうこう しゅうこう しゅうしょうしょう しょうしょうしょう しゅう はごうりょう しゅう はいりゅう しゅうしょう しゅうしょう しゅうしょう しゅうしょう しゅうしょう しゅうしょう しゅう しゅうしゅう しゅうしゅう しゅうしゅう しゅうしゅう しゅうしゅう しゅうしゅう	UN COPIE
MANANTE EMERICANO DE COME COMO DE COMO	COCKE
00 00 00 00 00 00 00 00 00 00 00 00 00	၁၀ဝဝဗဗဗ
ուր ոլորությունը արարարարարարարարի արարարարարարարարարարա	<u>பயய்யியம்</u>
- アンプラントライク・アン・ストール といって とうしょう とうしょう とうしょう とうしょう しょうしょう しょうしょう しょうしょう しょうしょう しょうしゅう しょうしゅう しょうしょう しょうしゅう しゅうしゅう しゅう	0.00 CO 000 CO
WARRENDER TO WARRE TO A STATE OF THE PROPERTY	1W (0 60) V (V)
4000000000000000000000000000000000000	4m4m4n
The state of the s	200000
ちゃほとうそ ひごうずほごうてきごうかん ほうかん はっちゅう はっちょう はっちょう はっちょう もっちょう もっちょう もっちょう もっちょう はっちょう はいい はい	invesion.
More to the state of the state	こうしょうしょうしょうしょう しゅうしょう
and the strategic for the second of the seco	

Table A1. Listing of COMBH2O Band Model Parameter Set (Cont'd)

SC COCCO SC		
um minimin		
mornon.	ŧ	- පරස්තයක් අත්තයක් නියක් නියක් අතර පස්තය සහ
のよれてころで	•	しょうこうこうこう ちょくくろう ちらんごう うごうしょう しょうしょうしょう とくしょう しょうしょう しょうしゅう
• • वं • • • च्यानाचीच्याच्याच्या	•	
MMMMEE		
000000		
		= + * + + * + * + * + * + * + * + * + *
500 C C C C C C C C C C C C C C C C C C		00000000000000000000000000000000000000
らう ロロ よう		topathored and order and companies of the companies of th
٠٠٠ ١		
tttk tt		
000000		
ا بالبنا لبنا لبنا لبنا البلاينا		անական անականանի անական անական կանական անանի անանի անանան անագարան ա
175 to		winsongains a daonile and assance and a tagenda and a raise and a confidence and a confiden
שאי ה מיומיונה		tions of the series of the ser
מימי ששי מימי		- HAMMANINE TET FOUND OF THE COMMON AND THE PROPERTY OF THE PR
**************************************	•	
CA MOUNT		- arignariante de participa de la composição de participa de composição de la composição de la composição de c
800 d 100 D		ord or the transmonder the properties of the contract of the c
mm mmnini		· · · · · · · · · · · · · · · · · · ·
4+ 4+1011		nadaanda radaaadaaadaandaaadaaadaaadaaadaaadaaada
	ļ	- 0000000000000000000000000000000000000
	i	
シンヤマンナ	1	AND SOURCE AND COLOR TO SOUR SOUR SOUR SOUR SOUR SOUR SOUR SOU
OF WW VIQ.	İ	พระมางองคระจัดเกิดของคาการคายกา
WH HADE	i	้ายายายการและ เป็นเกาะ เป็น เป็นเกาะ เป็นเกาะ เป็นเกาะ เป็นเกาะ เป็นเกาะ เป็นเกาะ เป็นเกาะ เป็นเกาะ เป็นเกาะ เป
กหณากหก		, ode codepede octobede edebede edebede edebede edebe
		- + + + + + + + + + + + + + + + +
ちまるよれてにはここと		antinutulla alabara da
20 3 4 4 CO	! !	anticontrol of the control of the co
	: 1	
3m chount		- cimmononologues de la propertiona del propertiona della properti
000000 000000	់ ភូ:	
	1 1	* * * * * * * * * * * * * * * * * * *
MO NO OH	l o	DAMOS SADVINS ALLO PEDES AMALDAS DANA PROMODANA POR ALA PROMODE ALA PORTA PORT
44 G C W C	18	unduntodonalonoalna olda andan erate teata and uno offer and one
המשושה	ž į	ုပ်လို့မြို့လိုက်တို့လို့ တို့တို့ အလိုက်တို့ အလိုင်းသို့ လို့လို့ လို့လိုင်းသို့ မြောင်းကျွန်းသည်။ လို့လို့မှုလို့ မလို့လို့ လို့လို့တို့ လို့လို့တို့ လို့လို့သည်။ လို့လို့လို့သည်။ လို့လို့လို့လို့သည်။ လို့လို
ינית יער יגיע		יר המספטים בי ההחמים מרחה ל-ים או אום בי או או או מספי מספר מספר
00000	>	
محران مراب الناف	₫	
らてようよら	DC	
C-C) 4 (4 %	<1	
Chiate LUIT	2	
0000000 7777	<u>ک</u>	
11111		+ + + + + + + + + + + + + + + + + + + +
CO REPORT	H.	reversed of value and a weather when a drock the reduce were controlled and a drock and a drock that are
できる とう はらり はっちょう しゅうごう しゅうごう しゅうごう しゅう	25	らった。ちょうちょうらうころでしょうかんらいちょうとうちょうりょうしょうしょうしょうしょうしょうしょうしょうしょうしょうしょうしょくらんさん はんちょうしょ はんきゅん はんかい しゅうしょう ステート・スログ まはしい
TOWN UT	c.	$\begin{array}{c} \bullet
מימי מו מי נדי	쁘	
000000	- + }	17111111111111111111111111111111111111
tite tilliatete.	ا لـ	
100 M 00 C C C	VE	eodaeontronamentalenen attachen en anteres anteres en a
wood viou	9-3 9	
nwalalan	ပ္	randermontos en al manda de la manda del manda del manda de la man
ocide oe	្រ រ	
000000	ir (
25,25,25	İ	OUNT OUNT OUNT OUNT OUNT OUNT OUNT OUNT
UP TE E EM		とのことととところところとととととととととととととというところころころころころころできるととところとは、それは、日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の日
,	ı (

ਰ
r Set (Cont'd)
Set
. Parameter
nd Model
of COMBH2O Band Mod
Listing
Table A1.

THE PERSON NAMED IN

高速度等的工作。

Salar Salar

自身

	domando
	200000
ໝໍເນີນເມັນເປັນເປັນ ເປັນ ເປັນ ເປັນ ເປັນ ເປັນ ເປັນ	نىل اندانىلانىلانى
ONGO PENDENG A LA COMBRAGA CON CONTRA CON CONTRA CON CONTRA CON CONTRA	ようよるア ロ
on and the man de 40000	
	i 1
	99999
	<u>ப்றார்</u> ம்
- 000000000000000000000000000000000000	200200
m dr ua dra a do dr r a dr u dr u dr u dr u dr u dr u dr	4040,000
++++++++++++++++++++++++++++++++++++++	
້ານທີ່ເປັນພັນດີເປັນພັນ	<u> </u>
こうらんしゅうしょうしょうしゅう しょうしょう シェント・コント・コント・コント・コント・コント・コント・コント・コント・コント・コ	することりと
การที่สามารถสามารถสามารถสามารถสามารถสามารถสามารถสามารถสามารถสามารถสามารถสามารถสามารถสามารถสามารถสามารถสามารถสา สามารถสามารถสามารถสามารถสามารถสามารถสามารถสามารถสามารถสามารถสามารถสามารถสามารถสามารถสามารถสามารถสามารถสามารถส	# * * * * * *
and the december of the decemb	•
** + * + * + * + * + * + * + * + * + *	20000
ເນັ້ນເປັນເປັນເປັນເປັນເປັນເປັນເປັນເປັນເປັນເປັ	TICLE TO COMPANIE TO THE COMPA
TO THE TO THE TOWN THE TOWN TO	~ ろうよろこ
	1
######################################	
OF STANDER OF STANDER	立 こ る フ テ
and conditions are an an an an an an an an an an an an an	4 4 -
	1
	<u> </u>
كالمكيب ليبألف فدناف فيتألف ليدا لمتألف ويداف فيألف ليبالف للمؤلف ليداف لماليا أشد لفنافيا لمرأف الدالية الما	.վականակե
is awind we is a sold the compact in a will the completion of the completion of the compact is a sold of the compact in a sold of the compact is a sold of the compact in a sold of the compact is a sold of the compact in a sold of the compact is a sold of the compact in a sold of the compact is a sold of the compact in a sold of the compact is a sold of the compact in a	いてのらと
	ન્•••ન્•
	1
	dooodo
	ا بالبالبالبالباربال
ころらりずんとのするのこをくも自てころとを作りてしたとをを見る!	ひてまるので
ENDERGY OF THE PROPERTY OF THE	-lo o cm -
	decede
i da didicia di di di di di di di di di di di di di	THE WELL
MANA COMPANDIO DE LA COMPANDIO	4 c c c c c c c c c c c c c c c c c c c
	de a roll
	1
SOURCE STORES AND SOURCE STORES AND SOURCE STORES ON SOURCE STORES AND SOURCE STORES ON SOU	
NUMP Ga MUNALP Q WAS A SO SO SO SO SO SO SO SO SO SO SO SO SO	chrucha
70 30 NO NO NO NO NO NO NO NO NO NO NO NO NO	11111
ov doe ocloood-toedrop-oclooodoodoodoodoodoodoodoodoodoodoodoodoo	HIP TO BE COLUMN
- 日ではするできることできるとのできました。 - 日では、日本は、日本は、日本は、日本は、日本は、日本は、日本は、日本は、日本は、日本	30000000000000000000000000000000000000
· · · · · · · · · · · · · · · · · · ·	400001
	00000
AT THE TEACH OF THE THE THE THE THE THE THE THE THE THE	200000
No Novo No	192200
หมายพบบบบบบบบบบบบบบบบบบบบบบบบบบบบบบบบบบบบ	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
	•

NINNONNAN 7.05.20 5.7.20 5.7.20 5.7.20 5.0 ô 5 アンプラウュラウア <u>~1</u> 20000000 VIVIDAGENE SIDAMAN SIDAMAN TO THE SIDAMAN TO THE SIDAMAN SIDAMAN TO THE SIDAMAN SIDAMA -320ADENI SELF VON-RESONANT in' C) ili THE ARGAYICH-17ATH, 6-0386-02 7-05876-102 7-0866-102 7-7866-102 7-102 7-102 7-102 7-102 5.04.2E-02 7.83.97F-02 7.63.96E-02 7.63.46E-02 7.64.6E-02 7.64.6E-02 6.96.7-02 WIDTHUR LINE HEAV

000000000

-51-

			+++++++++++	1 0	1	27-14-07-18-14-18-18-18-18-18-18-18-18-18-18-18-18-18-
!	! ;		terbeilettettetteilettettettettettettet	i iii		004600-424-000
				98		Manuteteman
			しょうらきしゅうかん	0		สตเลตเลตเลเลเลเล
1		!	- mmmmmmmmmmmm	m		000000000000
	1	!	MANAGEMENTANTANTANTANTANTANTANTANTANTANTANTANTAN	m	j	
i		1		9	i	ととててもものものようです
1				1 8		P. Com China Richard
i			ちゅうちゅうちゅうちゅうちょうちょうちょうちょうちょうちょうちょうちょう	0		o mandamental con con
İ		;	• 여 • • • 이 • • • 이 • • •	r.		tettettett
į	1	Ì	mmmmmmmmmmm	~	1	1111111111
-	:	1		33		mmmmmmmmmmmm
:		1	++++++++++++++	+		ちろうてもこうなりとうなっ
!			reminental protection and the second	10		0043430034000
			MONONOR MONON	80		ONUMBER TUMOO
:	:	1	MMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMM			++++0000000000000000000000000000000000
	1		MMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMM			
i	!		+++++++++++		1	
;		i	មាជាការការការការការការការការការការការការការ	! 👛	i	のようまでものもまたと
ļ				0.0		mmm+wmmon
!	(1	しているというない	.5		1 1 ' 1
		! !	พพพพพพพพพพพ	1,1		- coopeanone
ļ	: .	;	๛๛๛๛๛๛๛๛๛๛๛	m		
,		i	+++++++++++	! •		00000000000000000000000000000000000000
			ուսիս է բուլուս և Արև և Մարև	l L		ようようちょうらってよるち
!	1 !	i	orive or or or or o	00		
	; .	1	4-100mm 3310000r			การางกรายกรายกรายกรายก
į	d ∽ '	1	wishen was was ware	*+		
·	2000 ·	!		0.5	}	นั้นเป็นเป็นเป็นเป็นเป็น กลุ่นเพื่อเลของจอง
	93030	•	· + + + + + + + + + + + + ++	1 +		TOURON TO TOUR CO
	HUOOOO			O		いいましたようというよう
:	ZZZZZ	1	よりとうとしているととしてといって	20	1	worker and acception
: ;		;	MMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMM		ļ	220000000000000000000000000000000000000
1 i	00000	!	1 1 1		_	
	ಎರ್ಎಂಎ⊄		00000000000000000000000000000000000000	02	E	
1 1	T SISSES	(2)	++ ++++++++++++++	10 F + 3	\ \	H00-0000000000000000000000000000000000
· ;	ยี่พงพที่ยี	4		9	1	-om-mange-
1 1	CCCC	7	まれたころできるようない	11 0	1 X.	
1	F-1 1.1 (34)	2	mmmmmmmmmmm	N 7	2	000000000000000000000000000000000000000
	AGGGGG		๛๛๛๛๛๛๛๛๛๛๛๛	~	A	
a			++++++++++++	0	α,	00040044000 00000440000
22	co vialatarara			li.	44	たらからのなけるのでものは
(3)	C) O'LLLLL, 407	극	HIGHOHOHOHOHOHOHO	χ 0 0	_	ant mon-atomata
भ	r i	 	まるころではいること	2 <u>1</u> 0	×	2000 11 11 10 10 10 10 10 10 10 10 10 10
3		4	mmmmmmmmmmm.n	~ 0	 	
\ v. \	50 500	A		A C 0	IE	
l o.		Ωri		0.1 +	101	4-manummanumin
- I	2 2	•<	TOTAL OF THE PROPERTY OF THE PARTY OF THE P	4 0	l L	THE CHANGE CHANGE TO A CONTRACT CONTRAC
Y :	1 4M M44			2 6	in in	and the contraction
4 2	# N X	Z	MMMMMMMMMMMMMMM	= :	00	4404444600000 667460000000
4		-	mmmmmmmmmmmm	ATURE(E+02 2	1	
ا بر		<u>u</u> }	+++++++++++++	5 5	NO	30-00034000000
- LU F		X)	فبالمأليانيانيانيالياليالياليانيان	E +	11	11000000000000000000000000000000000000
' O 20-	ા વાલાવાનાના	22.		90	a or	44-40-401-100-10-0
7 2	000000	Š	A A CINIMIN TO THE CONTRACTOR	Č 0	53	
2 3	X 44444		๛๛๛๛๛๛๛๛๛๛๛๛๛	<u>.</u>	60	
88 NS		7				ananananana
	1					DOMESTINE STAND
1	1	l				en man an an an an an an an an an

Table A2. Listing of COMBCO2 Band Model Parameter Set

 	- International and a series	dana ada and a a a a a a a a a a a a a a
**************************************	ମ୍ବର୍ଷ ବ୍ୟବ୍ୟ ଦେଇ ପ୍ରଥମ ବ୍ୟବ୍ୟ ଦେଇ ପ୍ରଥମ	
マック くんしゅん しゅんりんしゅんけんけん	3/8/2013/1/ アクファクアングラング (1) (1) (1) (1) (1) (1) (1) (1) (1) (1)	๚๛๛๛๚๛๛๛๛๛๛๛๛๛๚๛๛๛๚๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛
こうけんしゅうしゅうしゅう こうしょうしゅう	マット・マー・マー・ストン しょうしょう しょうしん	- のとうともを与された。中とうようないできるものとととららなくれて、ころりとよるをできれた。 ちょうしょう こうしょう しょうしょう しょうしょう しょうしょう しょうちょう しょうりょう
no my respectations	. 64 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	
		donadamadamadamadamadamadam
- 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	?! ? 8 £ 2 1 8 0 0 4 6 1 E 8	/m/nm/mm/mm/mm/mm/mm/mm/mm/mm/mm/mm/mm/m
- was too to see with which each of the self of the read of the re	えでこうりゅうろく こうぐしりょうろうこう こうこういい	- + @70 @ AM @ O D @ O D D AM @ C D D O O O O O O O O O O O O O O O O O
an end a conductive to a con-		4.0.0.0.0.4.4.5.0.0.0.0.0.0.0.0.0.0.0.0.
Tadah Marana		designation of the second of t
- 60 (60 00 00 00 00 00 00 00 00 00 0	460666000066000	de de de de de de de de de de de de de d
	(Անհերին ին և ին հետ ին ին ին հետև ին հետ ին հետև ին և ին հետև ին հետև ին հետև ին հետև ին հետև ին հետև ին հ	1 ω ω ω ω ω ω ω ω ω ω
~ והאונוט הגולול) כבון עבור עלול (לו) ובוט הובו ולולונו על וואול	<u>ものいいかん きんりのかいべ</u>	<u>イルト・ストトーᲚᲝᲙᲔᲚᲚᲚᲡᲠᲑᲝᲑᲡᲚᲑᲥᲑᲡᲚᲠᲑᲡᲚᲑᲠ</u> ᲚᲡᲘᲡᲡᲑᲚᲡᲑᲚ
Mrs aller to aller entertertente	ME F F WMMININININI	Induct of war and an and the analysis of all of
entrick to the terminal control of the control of t	ma e electroler ele	THE PROPERTY OF THE PROPERTY O
	5 4	
しょうきょうしょうしょうしょうしょうしょうしょう	よるり らこう うううごう うて	#(V) D/V イアのもなうちゃんできることとなるのまちゃんかんかん はっぽうちょう しょうしんちょくしゅう ちょうしょう はいしょう しょうじょうしょく しょうしょう しゅうしょう しゅうしょう しゅうしょう しゅうしょう しゅうしょう しゅうしょう しゅうしょう しゅうしょう
- **** (単位 (ごう) (よう) らき (はこう) うきん	うらんりょう 4 まりりんりん	WARDHALL MUNDA BLA HOD GHUAN WOOWHNA
רש עייו איי איי איי איי איי איי איי איי איי	ון שנונות איי אונינל הי שנעים	fundadamm + Alvordendendendendens
ada elo be el a el el el elo como nun idio inio idio inio idio inio ini	10000000000000000000000000000000000000	~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~
- ան անաև և անանանանան	, ապանանական անև	[D]
- 名子 ごすりこう ユア こうりょう 4 31	くらりひりうことままり	でいる自由できますが、自己では自己できません。
_ ^ -	4 * * * 4 * * * 4 * * * 4	THE STANDARD TO BE THE STANDARD TO SEE THE STANDARD TO SEE THE SEC THE
	1 i 1 1	EEEEEEEE NAINEEEEEEEE NEDA NAEEAN
	11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
トランジをていらい くくこうしん	エよりりょうそうひょうりご	<u> </u>
・ さいりゅうこうりょうこうこうしょうしゃ	さけとこり こうてき とうこうけい	
oo do co do ao do oo do oo do oo do oo do oo do oo do oo do oo do oo do oo do oo do oo do oo do oo do oo do oo	7 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	+ + + 100000000000000000000000000000000
しゅうきゅうえきゅうしょりゅう	O CO CO CO CO CO CO CO CO CO CO CO CO CO	๛๛๚๛๛๛๚๛๚๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛
	4 • • • 4 • • • 4 • • • 4	$\mathcal{L}_{\mathcal{L}}}}}}}}}}$
A 40 aproximitation aprior	a arriariod	annanablananananan art raada can
The munimum number	a Horomonia	2000 200
各とような日本ではアファファア	ರ್ಷ- ವ⇔ರಲಗೂರ್ಯನ್ನ	45.50.20.20.20.20.20.20.20.20.20.20.20.20.20
ועם עוד של בו בו שונו של ביו ביו	RODA HUMUNO HM	a Hound Hand Land Hound Hand Land And And And And And And And And And A
pa do op op op op op op op op op op op op op	o doobda aad	4 000000000000000000000000000000000000
- 11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		1 1 1 1 1 1 1 1 1 1
000 10 0 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	a Marchamery.	<u>ヰヰとてもできならよってきょりというおんまりまとうよってらっています。 マース・ストラステスト まましょう しょうりょう はん ちゅう はまない はましょく はましょう しょう はいい はい はい はい はい はい はい はい はい はい はい はい はい</u>
MU-UNE SAMPRONANO	III CONDUSTIBLE	OCHMONICONOCHED ON OCHMONICONICONICONICONICONICONICONICONICONIC
100 INTONTONOR MESTIN	i	VVUQUUNITATATUNDOOOOOOOOOOOOOOOOO
00 00000000000	4 440000000	
EIN MINIMUM MI	w	գ
RESIDENTA OF THE STATE OF THE S	N micror characteristic materials	ap-Hundont-oc-to-sul-co-rus
るのようというような	• • • • • • • • • • • • • • • • • • •	ทุกของการ
en du accionado do cod	CO CCC CCCCCCCCCC	000000000000000000000000000000000000000
No Novo Novo Novo Novo	မာက်မာက်မာက်မာက ျှောက်မာ က	ADVOVANDADATONAMOMMANAMOMMANAMOM AT A TERT TO DO DO DO ON AND AND AND AND AND AND AND AND AND AN
ますままますころろろろろろろろろろろろろう。またのののののはままたろろろろろ	とろうころろろろろろろろろろろろう	BD-4-00000000000000000000000000000000000
hame when serior indicates to the test to the test. but	אין אין נא נא נא נא נא נא נא נא נא נא נא נא נא	mentana mendena

Table A2. Listing of COMBCO2 Band Model Parameter Set (Cont'd)

- 7 4 7 2 7 4 4 4 4 4 6 4 1 0 4 1 0 4 1 4 4 4 1 1 1 1 1 1 1 1 1	9 8
E CONTRACTOR AND A CONTRACTOR AND A CONTRACTOR AND AND AND AND AND AND AND AND AND AND	ฅ๛๛๚๛ฅ๚๚๚๛๛๛๛๛๛๛๛๛๛๛๛๛ ๚๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛
and and all the terminate the management of the form o	พลสะระยะ
an na nada nada nada nada nada nada nad	
	4 4 4 6 6 4 4 6 6 7 4 1 1 1 9 7 7 7 7 1 1 1 1 1 1 1 1 1 1 1 1
うなりょうりゅうとうしょうりゅうらんこうくくうてる キェントロン ちょうしょうりょうりょうしょうしょうしょうしょうしょうしょうしょうしょう ちゅうちゅうしょう ちゅうちゅうしょう しょうしょうしょう しょうしょう しょうしゅう しょうしゅう しょうしゅう しゅうしゅう しゅうりゅう しゅうしゅう しゅうりゅう しゅうしゅう しゅうりゅうしゅう しゅうりゅうり しゅうしゅう しゅうしゅう しゅうしゅう しゅうしゅう しゅうしゅう しゅうしゅう しゅうしゅう しゅうしゅう しゅうしゅう しゅうしゅう しゅうしゅう しゅうしゅう しゅうしゅう しゅうしゅう しゅうしゅう しゅうしゅう しゅう	アスチロとてようないということのちらでではロロロチョンアとロロロタタカロらともですますのであるかって
SONOTOR ATTURE AND ACTUAN ANTENNE NO COTOR	
an an an analana da na analana analana analana analana analana	alananiananiananiananiananiananiananian
ごろんしょうしょ くんりょうしゅうしゅうしょうしょう としょくちょうしょく くんしょく としょく ちょうしょうしょうしょうしょうしょうしょう ストール スティング・ション・ストール スティース・スティースティースティース・スティース・スティース・スティース・スティース・スティース・スティース・スティース・スティース・スティース・ステ	- とりよっとこ えきちょうしゅ くらずっとなればらってると
maniste e e e e e e e e e e e e e e e e e e	
00000000000000000000000000000000000000	4 4 4 5 4 4 4 5 5 5
ごうほうごう コラステラ こうしょうしょう インシャン ション・ション・ション・ション・ション・ション・ション・ション・ション・ション・	- もますからられることととららずならららられる
and mander of the second of th	なできょうできょうとうじょうしょうてきょうしょう
momentalinadional trata to the trata a samurandional	
- 11 11 11 11 11 11 11 11 11 11 11 11 11	
MANAGEM AND AND AND AND AND AND AND AND AND AND	とう アスステ きょうらん りらてよう ままこうりょよう
すられてこのもれてものとくというというというとっているというというというというというというというというというというというというというと	
manding and and ordinary and ordinary and and and and ordinary and and ordinary and and ordinary and and ordinary and and ordinary and	
ปักษณ์สามายกายกาย เกาะสามายกายการทางการทางการทางการทางการทางการทางการทางการทางการทางการทางการทางการทางการทางกา เพลาะการทางการทางการทางการทางการทางการทางการทางการทางการทางการทางการทางการทางการทางการทางการทางการทางการทางการ	プログラウエア は しょう そうする ちょうしょう しょうりょう
	THO THE COLOND CONDUCTION
	30000000000000000000000000000000000000
/ Մանական անական անական արև Իրանանան արանան արանան արանան արանան արանական արանանան արանանան արանանան արանանան	~ ĸ~a~c>v M~a~a\a~a\b~a\b~a\b~a\c~a~a\c\c.~a x IIIII IIIIIIIIIIIIIIIIIIIIIIIIIIIIII
A COMPANDING TO A COLON AND TO A COLON AND TO A COLON AND A COLON	บ็ณ้วานในของใจจะสุขาดที่จะพริเริ่ง
· Mendo ou out the same of the month of the	FUND VINKAN WITH THE MARKET OF LOWER
errebereberado ordina ama amateteteta un un electro de de decembro de desenta amateteteta de de electro el la la la la la la la la la la la la la	
Jundulurudululululuruduluruduru duke ali du du du da da da da da da da da da da da da da	-
AWARE SHORE OF HOME HAS AND SHORE SHOWEN SHOWER OF THE STATE OF THE ST	さいのとうとうというというとうというとうという
מה מה ביו שני של ביו היו היו ביו ביו שני של מי ש	
orthorreposition and analysis to the residing of the section of th	adocode a adocode a code a
uddada aa ahaddadada gaabhaaaadhaaadaan ahaanaa ahaanaa ahaanaa ahaa ah	Na acologo acologo acologo de la maria la maria la maria la maria la maria la maria la maria la maria la maria
at deposition of the second of the side to the second of t	STANDONO CONTRACTOR CO
3日の日本ででは、1000円では、1000	decelemente de la compansión de la compa
	ころりて はつうさむしょしょうこうらってごと ろてごろう
940010 tunice まちょうしょう とうりょうしょう くりんりゅうしょう とうしょう とっちょう くりん りょうしょう しょうしょう しょうしょう しょうしょう しょうしょう しょうしょう しょうしょう しょうしょう しょうしょう しょうしょう しゅうしゅう	ふまりょうちゅうはくりょうちゅうようらうきてきこうしょうてららしゅうちょいこうじゅう かまかいこうじゅん タルルクトログル
ar ar de de la la compania del la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania del la compania del la compania del compania del la compania del	y nother work and the second control of the
	de e e e e e e e e e e e e e e e e e e
Syrangaran Anglandarangarangarangarangarangarangarangar	10つきょりをちにも100アアを100のりの食むしましただち
มินิย์ผลิต นักสามากับกับกับกับกับกับกับกับกับกับกับ เลือน และ ค.ศ. ค.ศ. ค.ศ. ของเกตเลือน การและ ค.ศ.ค.ศ.ค.ศ.ค.ศ.ศ.ศ.ศ.ศ.ศ.ศ.ศ.ศ.ศ.ศ.ศ.ศ	~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~

(Cont'd) Set Parameter Model Band] COMBC02 ō. Listing A2. able

4.554E-02 2.534E-02 2.734E-02 2.008E-02 3.734E-02 3.734E-03

7.437E-02 6.741E-02 4.741E-02 3.379E-02 1.3316-02 5.406E-03

1.00 62 E - 01 1.00 67 E - 01 7.03 07 E - 02 5.32 07 E - 02 7.62 E - 03 7.66 2 E - 03

2.350E-01 2.350E-01 3.350E-02 3.350E-03 3.350E-03 3.350E-03 3.350E-03

2.4446E-01 3.54446E-01 2.356E-03 2.754E-04 1.15484E-04 2.036E-03

3.7.5.0.0 3.7.5.0.0 3.7.5.0.0 3.7.5.0.0 3.7.5.0.0 3.7.5.0.0 3.7.5.0.0 3.7.5.0.0 3.7.5.0.0 3.7.5.0.0 3.7.5.0.0 3.7.5.0.0 3.7.5.0.0

y.

ξ...

THE PRESENCE AND SECURE AND PROPERTY.

A RRAY (LINES/CM-1)

LINE

ECTIVE

EFF

<u>۲</u>					1	l .	i	1	1 1
	こうこうしん	(w) (w) (w) (w)	יא כיא ניא ניא ((M) (M) (M)	100 WW	さいらいき	さんさん くんしょ	100 MM	id to the total to the total total for
	0000	0000	COO	(0000	40000		(0000		
+	++++	++++	++++	(+ + + +	++++	+++	+++	+++	 +++ ++++ +
i.	بالنالعاليال	լաարա	عالينا لتناليا	عانيانيانيا	ياننا نباننا إ	յապատա	լաաաև	باساساسال	ក្រាហភាកាភាភាភា ភាពីវិសា
-	4-14-14-14-1	44444	44400	00 V- 10 V	1000	14000	OC MOOM	ൂയസ്⊣ാ	a war with with a color w
- 3	3222	2222	2260	UNIO CO 4	OWNO	WV-414	40/03/20	ကြောက်က မ	ay ⊷in'aiwci⊶iolo.o
,	town	10000	1000 C	10-10 NO	(N~ 00 CD +	100000	มเกรเพ	غص∼صو	0.400000000000000000000000000000000000
•	100000	10000	10000	444 444 444 444	4441011	liginicie	innonn	100000	から かった ひ ひ たい () () ()
				~~~~					7 40 40 40 40 40 40 40 40 40 40 40 40 40
								10000000000000000000000000000000000000	
		1111	7777	7777	1111	1 4 4 4 4	1111	1222	
L.	باشتشت	اساساسان	யெய்ய	www	أثاثاثاث	سسانسان	بنيشتين	بالنالناليا	ப்பய்யியியியியியியியியி
ir	minion	inspire	anine of	-IMM	NIA and of	00.40	10 M	0000	MALEMIAMAGINA
Ę.	MANAM	MMMM	mmine	0014-	OW ST	4000	12020	COOR	שורוט אד מומוס אדם
៤	minimu	(เกเกเกเก	ろうりゅう	3010	WM JU	minio	1400	0000c	とのまするようなと これではいまなまり これではいますると
•			• • • •					• • •	
-	والمراجع والمراجع	-	مه احد احد احد	***	<del></del>	4-4-4-4-4-4-4-4-4-4-4-4-4-4-4-4-4-4-4-4-	<del>  +4+++4+</del>	{ - 4 - 4 + 4 C	ายนายนายนายนาย เกาะเกาะเกาะ
	1 :	i	1	1	i	1			
~ ~	COOL	00000	0000	NON	MONIN	10000	10000	line with the	20000000000000000000000000000000000000
_		1111		0000	0000	10000			
				20103000	2.0.0	11.11.11.11.11			10. 10. 11. 11. 10. 10. 11. 11. 11. 11.
ď	80 00 00	000000	E &C	2000	CIN CIA	- C C C	CHOOLIC	00.4	SPP TEMPORATION TO THE SECOND TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION TO THE SECOND TEMPORATION THE SECOND TEMPORATION THE SECOND TEMPORATION THE SECOND TEMPORATI
ē	0000	0000	0000	MM MM	NN 103	C C 4	MONE	9500	100 COURS OF THILL
~	MUNICI	Nainia	CICION	97,010,0	00 CT	+ LONG	COULDE	COO	אם אסיטור אוטיטר
σ.	യയയ	«ν.«ν.«ν.«ν	∞00000	7	<b>~~~</b> ∞ ∞	<b>ቋን</b> ቁን ቁን ቁን	თითი	j <del>- 1 - 1 - 1</del>	44444444400 4401010 +10101000 4401010 +10101000
_		ا د. د د د ا		i	<b>.</b>		; (		
2	SOUN	SOUGH	NONO	2000	SININ	SOUN	2000	MINIO	
Ç.	1 4 4 4					7700		- C-C-C	
1:	ជាជាជាជាជា	in white	LILL TO		LULIU CO	in Line	Liberation.	111111111111111111111111111111111111111	in Tarte to the total and the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the contro
	0000	0000	0000	25.70	シナ シア	W. 400	CKKK	00.+-	1+0000++000=
Ē	Ert	ttt	***	4000	DIT. 100	100 H 3 K	0000	100 N 10-1	4600440004
Ē	tttt	tttt	****	t te	ហហហហ	ഗരാര്	~ ~ ~ ~	COH	<u> จะเกษาจอก</u> นะคเ
•	1 • • • 4								. ระบะ ระบะการที่ เพลเพลเพลเลา เพลเพลเพลเพลเพลเพลเพลเพลเพลเพลเพลเพลเพลเ
^	luviou	くうころう	VIVIVIA	こうこう	SULVIV	טיטוטיט	ろろりょ	UINNW	FER EMMMMPH
				i 3		1 1	1	i	
	1222						4444		<u> </u>
9	7575	5567	5555	5000		12553	5000	0000	10000000000
1.	land that	i i i i i i i i i i i i i i i i i i i	mumi	tion of the	militie	ti namini	i dididi	in inini	
=	0000	0000	0000	8980	£300	9779	9000	040	たったったとしたが
LC.	<b>www</b>	เกเกเหน	ちらての	O O HM	NOOM	60 mg	MOWN	OOCU	SUMPORTORE
Ö	0000	თთთთ	$\sigma\sigma\sigma\sigma\sigma$	o co co co	<b>~</b> © <b>~</b>	ままろろ	とせせら	50×0	3040M45Net
•		4							
1	www	www	<b>WWWW</b>	ちゃちら	なななな	たかとた	わりりり	アヤヤセ	
***	4444	44444			4-14-14-14-1		44 44 44 44	41444	
<u>_</u>	++++	1 4 4 4	7577	7777	++++	7777	1111		144444444
u.	ய்ய்யய	ய்யய்யி	ப்பய்ய	மயம்ப	ជាជាជាជា	time time	unitin	i mini	hindring transport
ō	5555	0000	00.40	D 410 80	0000	37+6	8000	0000	OW COLHWOMHE
ŭ	9339	6000	MARIO	80 ec ec ec	4000	ままるる	MUTON	0000	HOD END 10 UM
M	MMMM	MMMA	MMMM	mmmm	LMMO	+++	ナナナナ	IUTUTUTE	สดุตาก การเการายเการา
•	• • • •					• • • •			
+	• • • • <del>•</del>		4 6 6 4 444444	• • • • •	€		7 0 0 0 4-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	4-1-4-1-4-1-	11-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1
,									
,									
,									
,									
,									
,									
,									
,									
,									
4.007E+09	4.007E+00 4.007E+00 4.416E+00 5.023E+00	4.306E+00 5.322E+00 5.500E+00 8.12E+00	5.689E+80 4.462E+90 4.564E+90 4.72E+90	4.515E+00 4.938E+00 4.945E+00 5.951F+00	3.536E+00 4.313E+00 4.043E+00 4.050E+00	4.0500E+00 4.0500E+00 4.057E+00 4.057E+00	4.0715+00 4.0775+00 4.0845+00 4.0915+00	4.3000 4.1000 4.11000 4.11000 4.11000 4.11000 4.11000	24 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
08 4.0075+09	00 4.007E+00 00 4.007E+00 00 4.416E+00 00 5.023E+00	00 4.9660+00 00 5.322E+00 00 5.500E+00 01 5.812E+00	00 5.6896+00 00 4.4626+00 00 4.6647+00	00 4.515E+00 00 4.938E+00 00 4.945E+00 00 5.941F+00	00 8.536E+00 00 4.313E+00 00 4.043E+00 00 4.05E+00	00 4.050E+00 01 4.050E+00 01 4.057E+00 00 4.054F+00	00 4.071E+00 00 4.077E+00 00 4.084E+00	6. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4.	20000000000000000000000000000000000000
08 4.0075+09	00 4.007E+00 00 4.007E+00 00 4.416E+00 00 5.023E+00	00 4.9660+00 00 5.322E+00 00 5.500E+00 01 5.812E+00	00 5.6896+00 00 4.4626+00 00 4.6647+00	00 4.515E+00 00 4.938E+00 00 4.945E+00 00 5.941F+00	00 8.536E+00 00 4.313E+00 00 4.043E+00 00 4.05E+00	00 4.050E+00 01 4.050E+00 01 4.057E+00 00 4.054F+00	00 4.071E+00 00 4.077E+00 00 4.084E+00	6. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4.	00000000000000000000000000000000000000
08 4.0075+09	00 4.007E+00 00 4.007E+00 00 4.416E+00 00 5.023E+00	00 4.9660+00 00 5.322E+00 00 5.500E+00 01 5.812E+00	00 5.6896+00 00 4.4626+00 00 4.6647+00	00 4.515E+00 00 4.938E+00 00 4.945E+00 00 5.941F+00	00 8.536E+00 00 4.313E+00 00 4.043E+00 00 4.05E+00	00 4.050E+00 01 4.050E+00 01 4.057E+00 00 4.054F+00	00 4.071E+00 00 4.077E+00 00 4.084E+00	6. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4.	######################################
3E+00 4×007E+09	5E+00 4.007E+00 5E+00 4.007E+00 3E+00 4.416E+00 3E+00 5.023E+00	E + 0 0	3F+00 5.689E+00  E+00 4.462E+00  E+00 4.864E+00  E+01 4.472E+00	7E+00 4.515E+00 5E+00 4.938E+00 5E+00 4.945E+00 7E+00 5.951E+00	7E+80 8.536E+00 2.7F+80 4.313E+00 2.7F+80 4.043E+00 3.5F+80 8.8F+80 8.	5E+01 4.050E+00 5E+01 4.050E+00 5E+01 4.057E+00 5E+00 4.054E+00	5E+00 4.071E+00 5E+00 4.077E+00 5E+00 4.084E+00 5E+00 4.091E+00	4.300E+00 4.300E+00 5E+00 4.119E+00 5F+00 4.4338F+00	######################################
25E+00 4*007E+00	25E+00 4.007E+00 25E+00 4.007E+0 39E+00 4.416E+00 13E+00 5.023E+00	31E+00 4.966E+00 70F+00 5.322E+00 67E+00 5.500E+00 36E+00 5.812E+00	58E+00 5.609E+00 91E+00 4.462E+00 21E+00 4.664E+00 84E+01 4.472E+00	33E+00 4.515E+00 36E+00 4.998E+00 65E+00 4.945E+00 47E+00 5.961E+00	87E+00 8.536E+00 895E+00 4.313E+00 825E+00 4.043E+00 825E+00 88050E+00 88050	25	25E+00 4.071E+00 25E+00 4.077E+00 25E+00 4.084E+00 25E+00 4.091E+00	4.300E+00 4.300E+00 4.300E+00 25E+00 4.119E+00	33 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
225E+00 4.007E+09	225E+00 4.007E+00 225E+00 4.007E+00 639E+00 4.416E+00 413E+00 5.023E+00	331E+00 4.966E+00 870E+00 5.322E+00 167E+00 5.500E+00 736E+00 5.812E+00	35888400 5.6098400 5918400 4.4628400 9218400 4.8648400 6848400 4.4728400	7336+00 4.5156+00 3366+00 4.9986+00 2656+00 4.9456+00 9476+00 5.9516+00	287E+00 8.536E+00 495E+00 4.313E+00 225E+00 4.043E+00 225E+00 4.050E+00	225E+01 4.050E+00 225E+01 4.050E+00 225E+01 4.057E+00 225E+00 4.054E+00	2255+00 4.0715+00 2255+00 4.0775+00 2255+00 4.0845+00 2255+00 4.0916+00	4.300E+00 4.300E+00 4.300E+00 225E+00 4.119E+00	23.3.3.4.4.4.0.3.3.4.4.4.0.3.3.4.4.4.0.3.3.4.4.4.0.3.4.4.4.0.3.4.4.4.0.3.4.4.4.0.3.4.4.4.0.3.4.4.4.0.3.4.4.4.4
225E+00 4.007E+09	225E+00 4.007E+00 225E+00 4.007E+00 639E+00 4.416E+00 413E+00 5.023E+00	331E+00 4.966E+00 870E+00 5.322E+00 167E+00 5.500E+00 736E+00 5.812E+00	35888400 5.6098400 5918400 4.4628400 9218400 4.8648400 6848400 4.4728400	7336+00 4.5156+00 3366+00 4.9986+00 2656+00 4.9456+00 9476+00 5.9516+00	287E+00 8.536E+00 495E+00 4.313E+00 225E+00 4.043E+00 225E+00 4.050E+00	225E+01 4.050E+00 225E+01 4.050E+00 225E+01 4.057E+00 225E+00 4.054E+00	2255+00 4.0715+00 2255+00 4.0775+00 2255+00 4.0845+00 2255+00 4.0916+00	4.300E+00 4.300E+00 4.300E+00 225E+00 4.119E+00	23.3.3.4.4.4.0.3.3.4.4.4.0.3.3.4.4.4.0.3.3.4.4.4.0.3.4.4.4.0.3.4.4.4.0.3.4.4.4.0.3.4.4.4.0.3.4.4.4.0.3.4.4.4.4
225E+00 4.007E+09	225E+00 4.007E+00 225E+00 4.007E+00 639E+00 4.416E+00 413E+00 5.023E+00	331E+00 4.966E+00 870E+00 5.322E+00 167E+00 5.500E+00 736E+00 5.812E+00	35888400 5.6098400 5918400 4.4628400 9218400 4.8648400 6848400 4.4728400	7336+00 4.5156+00 3366+00 4.9986+00 2656+00 4.9456+00 9476+00 5.9516+00	287E+00 8.536E+00 495E+00 4.313E+00 225E+00 4.043E+00 225E+00 4.050E+00	225E+01 4.050E+00 225E+01 4.050E+00 225E+01 4.057E+00 225E+00 4.054E+00	2255+00 4.0715+00 2255+00 4.0775+00 2255+00 4.0845+00 2255+00 4.0916+00	4.300E+00 4.300E+00 4.300E+00 225E+00 4.119E+00	33 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
1.225E+00 4.007E+09	1.225E+00 4.007E+00 1.539E+00 4.416E+00 2.413E+00 5.023E+00	2.331E+00 4.956E+00 2.870E+00 5.32E+00 3.157E+00 5.812E+00	3.358F+UU 5.689E+UU 1.6921E+UU 4.462E+UU 1.921E+UU 4.465E+UU 1.684F+UU 4.472E+UU	1.733E+00 4.515E+00 2.35E+00 4.998E+00 2.265E+00 4.945E+00 3.947E+00 5.951E+00	4.287E+D0 8.536E+D0 1.495F+D0 4.312E+D0 1.225E+D0 4.043E+D0	1.225 E + 3 0 4.9 5 0 E + 3 0 1.225 E + 0 1 4.0 5 0 E + 0 0 1.225 E + 0 0 4.0 5 7 E + 9 0 0 4.0 5 4 E + 9 0 0 4.0 5 4 E + 9 0 0 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 5 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 E + 9 0 0 5 E + 9 0 0 5 E +	1.225 E + 00 4. 07 1 E + 00 1. 225 E + 00 4. 07 E + 00 1. 225 E + 00 4. 084 E + 00 1. 225 E + 00 4. 084 E + 00	0. 0.300E+00 0.300E+00 1.225E+00 1.325E+00 1.325E+00	2.178
1.225E+00 4.007E+09	1.225E+00 4.007E+00 1.539E+00 4.416E+00 2.413E+00 5.023E+00	2.331E+00 4.956E+00 2.870E+00 5.32E+00 3.157E+00 5.812E+00	3.358F+UU 5.689E+UU 1.6921E+UU 4.462E+UU 1.921E+UU 4.465E+UU 1.684F+UU 4.472E+UU	1.733E+00 4.515E+00 2.35E+00 4.998E+00 2.265E+00 4.945E+00 3.947E+00 5.951E+00	4.287E+D0 8.536E+D0 1.495F+D0 4.312E+D0 1.225E+D0 4.043E+D0	1.225 E + 3 0 4.9 5 0 E + 3 0 1.225 E + 0 1 4.0 5 0 E + 0 0 1.225 E + 0 0 4.0 5 7 E + 9 0 0 4.0 5 4 E + 9 0 0 4.0 5 4 E + 9 0 0 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 5 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 4 E + 9 0 0 5 E + 9 0 0 5 E + 9 0 0 5 E +	1.225 E + 00 4. 07 1 E + 00 1. 225 E + 00 4. 07 E + 00 1. 225 E + 00 4. 084 E + 00 1. 225 E + 00 4. 084 E + 00	0.	0 2 - 173 E + 0 3 5 0 2 + 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
-01 1.225E+00 4.007E+09	.01 1.225E+00 4.007E+00 -01 1.525E+00 4.007E+00 -01 1.639E+00 4.416E+00 -01 2.413E+00 5.023E+00	00 2-331E+00 4-966E+00 2-870E+00 5-322E+00 00 3-167E+00 5-812E+00	.00 3.358F+00 5.609E+00 00 1.921E+00 4.462E+00 00 1.921E+00 4.465E+00 00 1.684E+01 4.472E+00	.00 1.733E+00 4.515E+00 0.515E+00 0.525E+00 4.945E+00 0.5255E+00 0.5359E+00 0.5559E+00 0	.00 %-287E+00 8-536E+00 -01 1.495E+00 4-313E+00 -01 1.225E+00 4.050E+00	.01 1.225F+01 4.050E+00 -01 1.225F+01 4.050E+00 -01 1.225F+01 4.064F+10	.01 1.225F+00 4.071E+00 -01 1.225E+00 4.077E+0 -01 1.225E+00 4.074E+00	0. 4.30.00+00 0. 1. 225E+0.0 4.300E+00 0. 1. 225F+0.0 4.33F+0.0	++00 2-173E+00 5-024 +00 4-2439E+00 5-028 -01 1-2432E+00 5-0387E+00 -01 1-232E+00 5-0387E+00 +00 1-3237E+00 4-1889E+00 +00 7-27F+00 4-2865E+00 +00 2-649E+00 5-2656F+00 +00 1-455F+00 5-2666E+00 +00 1-455F+00 5-2666E+00 +00 1-455F+00 5-2666E+00 +00 1-455F+00 5-2666E+00 
-01 1.225E+00 4.007E+09	.01 1.225E+00 4.007E+00 -01 1.525E+00 4.007E+00 -01 1.639E+00 4.416E+00 -01 2.413E+00 5.023E+00	00 2-331E+00 4-966E+00 2-870E+00 5-322E+00 00 3-167E+00 5-812E+00	.00 3.358F+00 5.609E+00 00 1.921E+00 4.462E+00 00 1.921E+00 4.465E+00 00 1.684E+01 4.472E+00	.00 1.733E+00 4.515E+00 0.515E+00 0.525E+00 4.945E+00 0.5255E+00 0.5359E+00 0.5559E+00 0	.00 %-287E+00 8-536E+00 -01 1.495E+00 4-313E+00 -01 1.225E+00 4.050E+00	.01 1.225F+01 4.050E+00 -01 1.225F+01 4.050E+00 -01 1.225F+01 4.064F+10	.01 1.225F+00 4.071E+00 -01 1.225E+00 4.077E+0 -01 1.225E+00 4.074E+00	0. 4.30.00+00 0. 1. 225E+0.0 4.300E+00 0. 1. 225F+0.0 4.33F+0.0	++00 2-173E+00 5-024 +00 4-2439E+00 5-028 -01 1-2432E+00 5-0387E+00 -01 1-232E+00 5-0387E+00 +00 1-3237E+00 4-1889E+00 +00 7-27F+00 4-2865E+00 +00 2-649E+00 5-2656F+00 +00 1-455F+00 5-2666E+00 +00 1-455F+00 5-2666E+00 +00 1-455F+00 5-2666E+00 +00 1-455F+00 5-2666E+00 
-01 1.225E+00 4.007E+09	.01 1.225E+00 4.007E+00 -01 1.525E+00 4.007E+00 -01 1.639E+00 4.416E+00 -01 2.413E+00 5.023E+00	00 2-331E+00 4-966E+00 2-870E+00 5-322E+00 00 3-167E+00 5-812E+00	.00 3.358F+00 5.609E+00 00 1.921E+00 4.462E+00 00 1.921E+00 4.465E+00 00 1.684E+01 4.472E+00	.00 1.733E+00 4.515E+00 0.515E+00 0.525E+00 4.945E+00 0.5255E+00 0.5359E+00 0.5559E+00 0	.00 %-287E+00 8-536E+00 -01 1.495E+00 4-313E+00 -01 1.225E+00 4.050E+00	.01 1.225F+01 4.050E+00 -01 1.225F+01 4.050E+00 -01 1.225F+01 4.064F+10	.01 1.225F+00 4.071E+00 -01 1.225E+00 4.077E+0 -01 1.225E+00 4.074E+00	0. 4.30.00+00 0. 1. 225E+0.0 4.300E+00 0. 1. 225F+0.0 4.33F+0.0	++00 2-173E+00 5-024 +00 4-2439E+00 5-028 -01 1-2432E+00 5-0387E+00 -01 1-232E+00 5-0387E+00 +00 1-3237E+00 4-1889E+00 +00 7-27F+00 4-2865E+00 +00 2-649E+00 5-2656F+00 +00 1-455F+00 5-2666E+00 +00 1-455F+00 5-2666E+00 +00 1-455F+00 5-2666E+00 +00 1-455F+00 5-2666E+00 
-01 1.225E+00 4.007E+09	.01 1.225E+00 4.007E+00 -01 1.525E+00 4.007E+00 -01 1.639E+00 4.416E+00 -01 2.413E+00 5.023E+00	00 2-331E+00 4-966E+00 2-870E+00 5-322E+00 00 3-167E+00 5-812E+00	.00 3.358F+00 5.609E+00 00 1.921E+00 4.462E+00 00 1.921E+00 4.465E+00 00 1.684E+01 4.472E+00	.00 1.733E+00 4.515E+00 0.515E+00 0.525E+00 4.945E+00 0.5255E+00 0.5359E+00 0.5559E+00 0	.00 %-287E+00 8-536E+00 -01 1.495E+00 4-313E+00 -01 1.225E+00 4.050E+00	.01 1.225F+01 4.050E+00 -01 1.225F+01 4.050E+00 -01 1.225F+01 4.064F+10	.01 1.225F+00 4.071E+00 -01 1.225E+00 4.077E+0 -01 1.225E+00 4.074E+00	0. 4.30.00+00 0. 1. 225E+0.0 4.300E+00 0. 1. 225F+0.0 4.33F+0.0	34F + 00 2 - 178E + 03 5 0 2 4 E + 0 0 2 - 178E + 03 5 0 0 2 4 E + 0 0 6 - 10 0 4 4 9 E + 0 0 5 0 0 2 4 E + 0 0 0 2 1 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E
-01 1.225E+00 4.007E+09	.01 1.225E+00 4.007E+00 -01 1.525E+00 4.007E+00 -01 1.639E+00 4.416E+00 -01 2.413E+00 5.023E+00	00 2-331E+00 4-966E+00 2-870E+00 5-322E+00 00 3-167E+00 5-812E+00	.00 3.358F+00 5.609E+00 00 1.921E+00 4.462E+00 00 1.921E+00 4.465E+00 00 1.684E+01 4.472E+00	.00 1.733E+00 4.515E+00 0.515E+00 0.525E+00 4.945E+00 0.5255E+00 0.5359E+00 0.5559E+00 0	.00 %-287E+00 8-536E+00 -01 1.495E+00 4-313E+00 -01 1.225E+00 4.050E+00	.01 1.225F+01 4.050E+00 -01 1.225F+01 4.050E+00 -01 1.225F+01 4.064F+10	.01 1.225F+00 4.071E+00 -01 1.225E+00 4.077E+0 -01 1.225E+00 4.074E+00	0. 4.30.00+00 0. 1. 225E+0.0 4.300E+00 0. 1. 225F+0.0 4.33F+0.0	34F + 00 2 - 178E + 03 5 0 2 4 E + 0 0 2 - 178E + 03 5 0 0 2 4 E + 0 0 6 - 10 0 4 4 9 E + 0 0 5 0 0 2 4 E + 0 0 0 2 1 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E
445E±01 1.225E+00 4.007E+09	.481E-01 1.225E+00 4.007E+00 07E+00 0	.597E+00 2-331E+00 4-966E+00 108E+00 5-26E+00 5-167E+00 5-500E+00 5-966E+00 5-812E+00	.599F+80 3.358F+00 5.609E+00 -041E+00 1.691E+00 4.462E+00 -23E+00 1.921E+00 4.6564E+00 -033E+00 1.684E+00 4.472E+00	.074E+00 1.733E+00 4.515E+00 5549E+00 7549E+00 4.945E+00 2.265E+00 4.945E+00 7.22E+00 7.945E+00	.857E+00 4.287E+00 8.536E+00 .514E-01 1.495E+00 4.313E+00 .524E-01 1.225E+00 4.050E+00 .924E-01 1.225E+00 4.050E+00	.717F-01 1.225F+01 4.050E+00 .330E-01 1.225F+01 4.050E+0 .235E-01 1.225F+01 4.057F+00 .074E-01 1.225F+01 4.064E+10	.9155-01 1.2256+00 4.0716+00 .76%E-01 1.2256+00 4.0775+0 .619E-01 1.2256+00 4.0946+00 .502E-01 1.2256+00 4.0946+00		434F+00 2-174E+00 5-024E+00 7-024E+00 7-239F+00 5-087E+00 7-108F+00 5-087E+00 7-108F+00
9x445E=01 1x225E+00 4x007E+09	8.481E-01 1.225E+00 4.007E+00 9.887E-01 1.255E+00 4.007E+00 9.989E-01 1.639E+00 4.416E+00 1.672E+00 2.413E+01 5.023E+00	1.597E+00 2.331E+00 4.966E+00 2-108E+00 5.870E+00 5.402E+00 5.322E+00 2.405E+00 3.157E+00 5.812E+00	2.599F+80 3.358F+00 5.609E+00 1.041E+00 1.691E+00 4.652E+00 1.23E+00 1.921E+00 4.564E+00 1.033E+00 1.664E+00 4.6564E0	1.074F+00 1.733F+00 4.515F+00 1.549F+00 2.56F+00 4.945F+00 3.947F+00 5.951F+00	2.857E+00 4.287E+00 8.536E+00 7.504E-01 1.425E+00 4.043E+00 8.324E-01 1.225E+00 4.043E+00 8.324E-01 1.225E+00 4.050E+00	9.717F-01 1.225F+01 4.050E+00 8.330E-01 1.225F+01 4.050E+00 8.20E-01 1.225F+01 4.057E+00 8.074E-01 1.225F+00 4.064E+00	7.9155-01 1.2255+00 4.0715+00 7.7685-01 1.2255+00 4.0775+0 7.6195-01 1.2255+00 4.0845+0 6.5025-01 1.2255+00 4.0945+00		34F + 00 2 - 178E + 03 5 0 2 4 E + 0 0 2 - 178E + 03 5 0 0 2 4 E + 0 0 6 - 10 0 4 4 9 E + 0 0 5 0 0 2 4 E + 0 0 0 2 1 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E + 0 0 0 2 5 E
9x445E=01 1x225E+00 4x007E+09	8.481E-01 1.225E+00 4.007E+00 9.887E-01 1.255E+00 4.007E+00 9.989E-01 1.639E+00 4.416E+00 1.672E+00 2.413E+01 5.023E+00	1.597E+00 2.331E+00 4.966E+00 2-108E+00 5.870E+00 5.402E+00 5.322E+00 2.405E+00 3.157E+00 5.812E+00	2.599F+80 3.358F+00 5.609E+00 1.041E+00 1.691E+00 4.652E+00 1.23E+00 1.921E+00 4.564E+00 1.033E+00 1.664E+00 4.6564E0	1.074F+00 1.733F+00 4.515F+00 1.549F+00 2.56F+00 4.945F+00 3.947F+00 5.951F+00	2.857E+00 4.287E+00 8.536E+00 7.504E-01 1.425E+00 4.043E+00 8.324E-01 1.225E+00 4.043E+00 8.324E-01 1.225E+00 4.050E+00	9.717F-01 1.225F+01 4.050E+00 8.330E-01 1.225F+01 4.050E+00 8.20E-01 1.225F+01 4.057E+00 8.074E-01 1.225F+00 4.064E+00	7.9155-01 1.2255+00 4.0715+00 7.7685-01 1.2255+00 4.0775+0 7.6195-01 1.2255+00 4.0845+0 6.5025-01 1.2255+00 4.0945+00	0. 4.309E+00 5. 4.300E+00 6.918E-01 1.225E+09 4.119E+00 8.431E-01 1.225F+00 4.137E+00	1.434F+00 2.174F+03 5.024F+00 3.645E+00 4.429F+00 5.037E+00 5.037E+00 5.037E+00 5.037E+00 3.645E+00 3.645E+00 4.429E+00 4.845E+00 4.845E+00 4.845E+00 4.845E+00 4.845E+00 4.845E+00 4.845E+00 4.845E+00 4.845E+00 4.838E+00 4.8538E+00
9x445E=01 1x225E+00 4x007E+09	8.481E-01 1.225E+00 4.007E+00 9.887E-01 1.255E+00 4.007E+00 9.989E-01 1.639E+00 4.416E+00 1.672E+00 2.413E+01 5.023E+00	1.597E+00 2.331E+00 4.966E+00 2-108E+00 5.870E+00 5.402E+00 5.322E+00 2.405E+00 3.157E+00 5.812E+00	2.599F+80 3.358F+00 5.609E+00 1.041E+00 1.691E+00 4.652E+00 1.23E+00 1.921E+00 4.564E+00 1.033E+00 1.664E+00 4.6564E0	1.074F+00 1.733F+00 4.515F+00 1.549F+00 2.56F+00 4.945F+00 3.947F+00 5.951F+00	2.857E+00 4.287E+00 8.536E+00 7.504E-01 1.425E+00 4.043E+00 8.324E-01 1.225E+00 4.043E+00 8.324E-01 1.225E+00 4.050E+00	9.717F-01 1.225F+01 4.050E+00 8.330E-01 1.225F+01 4.050E+00 8.20E-01 1.225F+01 4.057E+00 8.074E-01 1.225F+00 4.064E+00	7.9155-01 1.2255+00 4.0715+00 7.7685-01 1.2255+00 4.0775+0 7.6195-01 1.2255+00 4.0845+0 6.5025-01 1.2255+00 4.0945+00	0. 4.309E+00 1. 6.918E-01 1.225E+09 4.119E+00 01 8.431E-01 1.225E+09 4.139E+00	01 1.434F+00 2.174F+09 5.024F+00 01 1.436F+00 0 2.239F+09 5.037E+00 0 3.639F+09 5.037E+00 0 3.645F+09 5.037E+00 01 1.51F+00 1.237E+09 4.413E+00 00 1 1.527E+00 1.8237E+09 4.417E+00 00 1 1.837E+10 0 2.645E+00 0 0 1.1837E+10 0 2.645E+00 0 0 1.1837E+0 0 2.645E+0 0 0 0 1.1837E+0 0 2.645E+0 0 2.645E+0 0 0 0 1.1837E+0 0 2.645E+0 0 2.645E+0 0 0 0 1.1837E+0 0 2.645E+0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
-01 9.445E+01 1.225E+00 4.007E+09	-01 8.481E-01 1.225E+00 4.007E+00 -01 9.989E-01 1.625E+00 4.416E+00 +00 1.639E+01 4.416E+00 +00 1.672E+00 +00 1.67	+0.7 1.5597E+00 2.331E+00 4.966E+00 2.00 2.108E+00 2.408E+00 3.157E+00 5.500E+00 4.00 2.408E+00 3.156E+00 5.812E+00	+00 2.599F+80 3.358F+00 5.609E+00 -01 1.041E+00 1.951E+00 4.561E+00 4.564E+00 -01 1.033E+00 1.684E+00 4.472E+00	-01 1.074F+00 1.733F+00 4.515E+00 -01 1.549F+00 2.25E+00 4.945E+00 +01 3.212E+00 3.947E+00 5.951E+00	+UN 2.857E+UO 4.287E+UO 8.536E+UO	-01 %.717F-01 1.225F+01 4.050E+00 -01 %.330E-01 1.225F+01 4.050E+00 -01 %.23E-01 1.225F+01 4.057F+00 -01 %.07F-01 1.225F+00 4.064F+00	-01 7-9155-01 1-2256+00 4-0716+00 0-01 7-5460 1-2256+00 4-0755+00 0-01 7-6196-01 1-2256+00 4-0946+00 0-01 5-2555+00 4-0946+00	0. 4.300E+00 0. 0. 4.300E+00 -01 6.918E-01 1.225E+09 4.15E+00 -01 8.431E-01 1.225F+00 4.133E+00	-01 1.434F+00 2.174E+00 5.024E+00 3.024E+00 3.729F+00 5.087E+00 4.498E+00 5.087E+00 6.428E+00 5.087E+00 1.151F+00 1.853FE+00 4.417E+00 1.853FE+00 4.817E+00 1.853FE+00 4.817E+00 1.853FE+00 4.817E+00 1.853FE+00 4.817E+00 1.853FE+00 1.853FE+00 1.853FE+00 1.831E+00 1.853FE+00 1.831E+00 1.853FE+00 1.831E+00 1.835FE+00 1.831E+00 1.835FE+00 1.831E+00 1.835FE+00 1.835F
E-01 9.445E-01 1.225E+00 4.007E+09	E-01 8.481E-01 1.225E+00 4.007E+00 E-01 9.87FE-01 1.629E+00 4.416E+00 E+00 1.639E+01 4.416E+00 E+00 1.672E+00 2.413E+01 5.023E+00	E+UJ 1.597E+UJ 2.331E+UJ 4.966E+UJ E+UJ 2.108E+UJ 2.870E+UJ 5.322E+UJ E+UJ 2.403E+UJ 3.156E+UJ 5.812E+UJ E+UJ 2.496E+UJ 3.736E+UJ 5.812E+UJ	E+UU 2.599F+UU 3.558F+UU 5.609E+UU 0.041E+UU 1.691E+UU 1.691E+UU 4.656F+UU 4.666F+UU 4.666F+UU 4.666FUU 4.672E+UU	E-01 1.074F+00 1.733F+00 4.515E+00 C-01 1.549E+00 2.236E+00 4.945E+00 C-01 1.533E+00 2.26E+00 4.945E+00 C-01 3.212E+00 3.947E+00	E+UN 2.857E+UN 4.287E+NN 8.536E+NN E-UN 8.536E+NN E-UN 1.495E+NN 4.313E+NN E-UN 7.495E+NN 4.315E+NN E-UN 1.225E+NN 4.05NE+NN 4.05NE+NN E-UN 1.225E+NN 4.05NE+NN E-NN E-NN E-NN E-NN E-NN E-NN E-NN	E-01 %.717F-01 1.225F+37 4.950E+00 F-01 8.330E-01 1.225F+01 4.057E+00 F-01 8.202E-01 1.225F+01 4.057E+00	F-01 7-915E-01 1.225E+00 4.071E+00 E-01 7.58E-01 1.225E+00 4.077E+0 E-01 7.519E+00 4.084E+00 E-01 6.802E-01 1.225E+00 4.084E+00	0. 4.309E+00 0. 4.300E+00 E-01 6.918E-01 1.225E+09 4.119E+00 E-01 8.431E-01 1.225F+00 4.134E+00	E-01 1.434F+00 2.174F+03 5.024F+00 E-01 1.436F+00 2.239F+03 5.037F+00 E-101 7.239F+03 5.037F+00 E-101 7.239F+03 5.037F+00 E-101 1.237F+03 4.17E+00 E-103 7.222F+00 4.237F+03 4.37E+03 E-101 1.495F+00 4.257F+03 4.538FF+03 4
E-01 94445E-01 1,225E+00 4,007E+09	E-01 8.481E-01 1.225E+00 4.007E+00 E-01 9.87FE-01 1.629E+00 4.416E+00 E+00 1.639E+01 4.416E+00 E+00 1.672E+00 2.413E+01 5.023E+00	E+UJ 1.597E+UJ 2.331E+UJ 4.966E+UJ E+UJ 2.108E+UJ 2.870E+UJ 5.322E+UJ E+UJ 2.403E+UJ 3.156E+UJ 5.812E+UJ E+UJ 2.496E+UJ 3.736E+UJ 5.812E+UJ	E+UU 2.599F+UU 3.558F+UU 5.609E+UU 0.041E+UU 1.691E+UU 1.691E+UU 4.656F+UU 4.666F+UU 4.666F+UU 4.666FUU 4.672E+UU	E-01 1.074F+00 1.733F+00 4.515E+00 C-01 1.549E+00 2.236E+00 4.945E+00 C-01 1.533E+00 2.26E+00 4.945E+00 C-01 3.212E+00 3.947E+00	E+UN 2.857E+UN 4.287E+NN 8.536E+NN E-UN 8.536E+NN E-UN 1.495E+NN 4.313E+NN E-UN 7.495E+NN 4.315E+NN E-UN 1.225E+NN 4.05NE+NN 4.05NE+NN E-UN 1.225E+NN 4.05NE+NN E-NN E-NN E-NN E-NN E-NN E-NN E-NN	E-01 %.717F-01 1.225F+37 4.950E+00 F-01 8.330E-01 1.225F+01 4.057E+00 F-01 8.202E-01 1.225F+01 4.057E+00	F-01 7-915E-01 1.225E+00 4.071E+00 E-01 7.58E-01 1.225E+00 4.077E+0 E-01 7.519E+00 4.084E+00 E-01 6.802E-01 1.225E+00 4.084E+00	0. 4.309E+00 0. 4.300E+00 E-01 6.918E-01 1.225E+09 4.119E+00 E-01 8.431E-01 1.225F+00 4.134E+00	E-01 1.434F+00 2.174F+03 5.024F+00 E-01 1.436F+00 2.239F+03 5.037F+00 E-101 7.239F+03 5.037F+00 E-101 7.239F+03 5.037F+00 E-101 1.237F+03 4.17E+00 E-103 7.222F+00 4.237F+03 4.37E+03 E-101 1.495F+00 4.257F+03 4.538FF+03 4
33E-01 9.445E-01 1.225E+00 4.007E+09 :	72E-01 8.481E-01 1.225E+00 4.007E+00 53E-01 9.877E-01 1.639E+00 4.416E+00 72E+00 78E+00 1.639E+00 4.416E+00 78E+00	12E+UJ 1.597E+UJ 2.331E+UJ 4.966E+UU 19E+UJ 2.4U7E+UJ 2.87DF+UJ 5.322E+UJ 5E+UJ 2.4U7E+UJ 3.156E+UJ 5.812E+UJ 22E+UJ 2.996E+UJ 3.736E+UJ 5.812E+UJ	11E+00 2.599F+00 3.358F+00 5.609E+00 11E-01 1.041E+00 1.921E+00 4.652E+0 11E-01 1.23E+00 1.921E+00 4.566+00 11E-01 1.03XE+00 1.924E+00 4.566+00	55E-01 1.074E+00 1.733E+00 4.515E+00 0.515E+00	78E+UN 2.857E+U0 4.287E+D0 8.536E+D0 17E-U1 8.536E+D0 4.95F+U0 4.043E+U0 17.225F+U0 4.043E+U0 17.225F+U0 4.050E+D0	38E-01 9.717F-01 1.225F+01 4.050E+00 54E-01 8.30E-01 1.225F+01 4.057E+00 27E-01 8.202E-01 1.225F+01 4.057E+00 21E-01 8.074E-01 1.225F+00 4.064F+00	14F-01 7.915E-01 1.225F+00 4.071E+00 26E-01 7.768E-01 1.225E+00 4.077E+0 38E-01 7.619E-01 1.225E+00 4.084E+00 88E-01 6.602E-01 1.225E+00 4.094E+00	0. 4.309E+00 0. 4.300E+00 17E-01 6.918E-01 1.225E+09 4.119E+00 13E-01 8.431E-01 1.225F+00 4.134F+00	35E-01 1.434F+00 2.174E+03 5.024E+00 1.2436F+00 5.037E+00 5.037E+00 5.037E+00 5.037E+00 5.037E+00 5.037E+00 5.037E+00 1.2436F+00 1.2437E+00 1.257E+00 1.257E
33E-01 9.445E-01 1.225E+00 4.007E+09 :	72E-01 8.481E-01 1.225E+00 4.007E+00 53E-01 9.877E-01 1.639E+00 4.416E+00 72E+00 78E+00 1.639E+00 4.416E+00 78E+00	12E+UJ 1.597E+UJ 2.331E+UJ 4.966E+UU 19E+UJ 2.4U7E+UJ 2.87DF+UJ 5.322E+UJ 5E+UJ 2.4U7E+UJ 3.156E+UJ 5.812E+UJ 22E+UJ 2.996E+UJ 3.736E+UJ 5.812E+UJ	11E+00 2.599F+00 3.358F+00 5.609E+00 11E-01 1.041E+00 1.921E+00 4.652E+0 11E-01 1.23E+00 1.921E+00 4.566+00 11E-01 1.03XE+00 1.924E+00 4.566+00	55E-01 1.074E+00 1.733E+00 4.515E+00 0.515E+00	78E+UN 2.857E+U0 4.287E+D0 8.536E+D0 17E-U1 8.536E+D0 4.95F+U0 4.043E+U0 17.225F+U0 4.043E+U0 17.225F+U0 4.050E+D0	38E-01 9.717F-01 1.225F+01 4.050E+00 54E-01 8.30E-01 1.225F+01 4.057E+00 27E-01 8.202E-01 1.225F+01 4.057E+00 21E-01 8.074E-01 1.225F+00 4.064F+00	14F-01 7.915E-01 1.225F+00 4.071E+00 26E-01 7.768E-01 1.225E+00 4.077E+0 38E-01 7.619E-01 1.225E+00 4.084E+00 88E-01 6.602E-01 1.225E+00 4.094E+00	0. 4.309E+00 0. 4.300E+00 17E-01 6.918E-01 1.225E+09 4.119E+00 13E-01 8.431E-01 1.225F+00 4.134F+00	35E-01 1.434F+00 2.174E+03 5.024E+00 1.2436F+00 5.037E+00 5.037E+00 5.037E+00 5.037E+00 5.037E+00 5.037E+00 5.037E+00 1.2436F+00 1.2437E+00 1.257E+00 1.257E
33E-01 9.445E-01 1.225E+00 4.007E+09 :	72E-01 8.481E-01 1.225E+00 4.007E+00 53E-01 9.877E-01 1.639E+00 4.416E+00 72E+00 78E+00 1.639E+00 4.416E+00 78E+00	12E+UJ 1.597E+UJ 2.331E+UJ 4.966E+UU 19E+UJ 2.4U7E+UJ 2.87DF+UJ 5.322E+UJ 5E+UJ 2.4U7E+UJ 3.156E+UJ 5.812E+UJ 22E+UJ 2.996E+UJ 3.736E+UJ 5.812E+UJ	11E+00 2.599F+00 3.358F+00 5.609E+00 11E-01 1.041E+00 1.921E+00 4.652E+0 11E-01 1.23E+00 1.921E+00 4.566+00 11E-01 1.03XE+00 1.924E+00 4.566+00	55E-01 1.074E+00 1.733E+00 4.515E+00 0.515E+00	78E+UN 2.857E+U0 4.287E+D0 8.536E+D0 17E-U1 8.536E+D0 4.95F+U0 4.043E+U0 17.225F+U0 4.043E+U0 17.225F+U0 4.050E+D0	38E-01 9.717F-01 1.225F+01 4.050E+00 54E-01 8.30E-01 1.225F+01 4.057E+00 27E-01 8.202E-01 1.225F+01 4.057E+00 21E-01 8.074E-01 1.225F+00 4.064F+00	14F-01 7.915E-01 1.225F+00 4.071E+00 26E-01 7.768E-01 1.225E+00 4.077E+0 38E-01 7.619E-01 1.225E+00 4.084E+00 88E-01 6.602E-01 1.225E+00 4.094E+00	0. 4.309E+00 0. 4.300E+00 17E-01 6.918E-01 1.225E+09 4.119E+00 13E-01 8.431E-01 1.225F+00 4.134F+00	35E-01 1.434F+00 2.174E+03 5.024E+00 1.2436F+00 5.037E+00 5.037E+00 5.037E+00 5.037E+00 5.037E+00 5.037E+00 5.037E+00 1.2436F+00 1.2437E+00 1.257E+00 1.257E
33E-01 9.445E-01 1.225E+00 4.007E+09 :	72E-01 8.481E-01 1.225E+00 4.007E+00 53E-01 9.877E-01 1.639E+00 4.416E+00 72E+00 78E+00 1.639E+00 4.416E+00 78E+00	12E+UJ 1.597E+UJ 2.331E+UJ 4.966E+UU 19E+UJ 2.4U7E+UJ 2.87DF+UJ 5.322E+UJ 5E+UJ 2.4U7E+UJ 3.156E+UJ 5.812E+UJ 22E+UJ 2.996E+UJ 3.736E+UJ 5.812E+UJ	11E+00 2.599F+00 3.358F+00 5.609E+00 11E-01 1.041E+00 1.921E+00 4.652E+0 11E-01 1.23E+00 1.921E+00 4.566+00 11E-01 1.03XE+00 1.924E+00 4.566+00	55E-01 1.074E+00 1.733E+00 4.515E+00 0.515E+00	78E+UN 2.857E+U0 4.287E+D0 8.536E+D0 17E-U1 8.536E+D0 4.95F+U0 4.043E+U0 17.225F+U0 4.043E+U0 17.225F+U0 4.050E+D0	38E-01 9.717F-01 1.225F+01 4.050E+00 54E-01 8.30E-01 1.225F+01 4.057E+00 27E-01 8.202E-01 1.225F+01 4.057E+00 21E-01 8.074E-01 1.225F+00 4.064F+00	14F-01 7.915E-01 1.225F+00 4.071E+00 26E-01 7.768E-01 1.225E+00 4.077E+0 38E-01 7.619E-01 1.225E+00 4.084E+00 88E-01 6.602E-01 1.225E+00 4.094E+00	0. 4.309E+00 0. 4.300E+00 17E-01 6.918E-01 1.225E+09 4.119E+00 13E-01 8.431E-01 1.225F+00 4.134F+00	1
Z.283E-01 9.445E-01 1.225E+00 4.007E+09	5.872E-01 8.481E-01 1.225E+00 4.007E+00 5.963E-01 9.877E-01 1.639E+00 4.0107E+00 4.158E+00 1.639E+00 4.416E+00 4.158E+00 4.58E+00 4.416E+00 4.158E+00 4.416E+00 4.158E+00 4.416E+00 4.158E+00 4.416E+00 4.416E+00 4.416E+00 4.416E+00 4.416E+00 4.416E+00 4.413E+00 5.413E+00 4.416E+00 4.418E+00 4.418E	1.212E+03 1.597E+03 2.331E+03 4.966E+00 1.419E+00 2.108E+03 2.2E+00 1.766E+00 2.407E+03 5.167E+03 5.530E+00 2.407E+03 3.156E+03 5.812E+03	Z.011E+00 Z.599F+80 3.358F+00 5.609E+00 7.411E-01 1.041E-00 1.951E+00 7.951E+00 4.6562E+00 6.341E-01 1.237E+00 1.921E+00 4.6564E+00 6.341E-01 1.033E+00 1.664E+00 4.672E+00	6.655E-01 1.074E+00 1.733E+00 4.515E+00 4.819E+00 4.8198E+00 4.819E+01 1.538E+00 2.265E+00 4.945E+00 2.240E+00 3.947E+00 5.951E+00	1.078E+01 2.857E+00 4.287E+00 8.536E+00 6.517E-01 8.504E+00 6.517E-01 7.245F+00 4.043E+00 5.501E-01 8.924E-01 1.225F+00 4.050E+00	5.203E-01 9.717F-01 1.225F+01 4.050E+00 5.664F-01 8.330E-01 1.225F+01 4.050E+00 5.492F-01 8.205E-01 1.225F+01 4.057F+00 5.321F-01 8.074E-01 1.225F+00 4.064E+00	5.114F-01 7.915E-01 1.225E+00 4.071E+00 4.926E-01 7.768E-01 1.225E+00 4.077E+0 4.739E-01 7.619E-01 1.225E+00 4.094E+00 3.558E-01 5.502E-01 1.225E+00 4.094E+00	0. 4.309E+00 1. 4.300E+00 3.907E-01 6.918E-01 1.225E+09 4.119E+00 5.803E-01 8.431E-01 1.225F+00 4.137E+00	9.185F-01 1.434F+00 2.174F+03 5.024F+00 5.174F+03 5.024F+00 5.239F+03 5.087E+00 5.239F+03 5.087E+00 5.239F+03 5.087E+00 5.239F+03 5.087E+00 5.237E+03 5.087E+00 5.836F+00 5.838F+00 5.237E+00 5.237E
18 7.283E-01 9.445E-01 1.225E+00 4.007E+09	10 5-872E-01 8-481E-01 1-225E+00 4-007E+00 10 6-652E-01 9-887E-01 1-525E+00 4-416E+00 10 6-652E-01 9-987E-01 1-639E+00 4-416E+00 10 1-538E+00 10 1-639E+00 10 10 10 10 10 10 10 10 10 10 10 10 1	10 1.212E+01 1.597E+00 2.331E+00 4.966E+00 10.419E+00 2.108E+00 2.407E+00 2.42E+00 1.766E+00 5.502E+00 1.766E+00 2.467E+00 5.500E+00 10.2.467E+00 5.500E+00 10.2.467E+00 5.812E+00	10 2.011E+00 2.599F+80 3.358F+00 5.609E+00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	10 6.655E-01 1.074E+00 1.733E+00 4.515E+00 10 4.515E+00 10 4.8998E+00 2.265E+00 4.9988E+00 1.537E+00 2.265E+00 4.945E+00 10 2.240E+00 3.947E+00 5.951E+00	30 1.078E+0N 2.857E+00 4.287E+00 8.536E+00 30517E-01 6.517E-01 1.495E+00 4.313E+00 4.517E+00 4.505E+00 4.505E+00 4.505E+00 4.505E+00 4.050E+00 4.0	10 6.203E-01 9.717F-01 1.225F+01 4.050E+00 10 5.664F-01 8.330E-01 1.225F+01 4.050E+00 10 5.492F-01 8.230E-01 1.225F+01 4.057F+00 10 5.321F-01 8.074F-01 1.225F+00 4.064F+00	10 5-114F-01 7-915E-01 1-225E+00 4-071E+00 10 4-926E-01 7-768E-01 1-225E+00 4-075E+0 10 4-35E-01 1-225E+00 4-084E+0 10 1-55E+0 10 4-084E+0 10 1-225E+0 10 4-084E+0 10 10 10 10 10 10 10 10 10 10 10 10 10	10 0. 4.309E+00 10 0. 1. 4.309E+00 10 3.907E-01 6.918E-01 1.225E+09 4.119E+00 10 5.803E-01 8.431E-01 1.225F+00 4.137E+00	9.185E-01 1.434F+00 2.174E+03 5.024E+00 3.125E-101 1.486E+00 2.239F+03 5.087E+00 5.125E-101 3.621E-01 4.498F+03 6.428E+00 10.2.058E+00 3.222F+00 1.855E+03 4.18E+00 2.058E+00 3.222F+00 4.687E+00 4.817E+00 3.239E-01 1.849F+00 2.649E+03 5.08E+00 1.102E+00 1.186F+00 2.649E+03 5.08E+00 1.172F+00 1.756F+00 2.638F+03 5.08E+00
10 Z.283E-01 9.445E-01 1.225E+00 4.007E+09	10 5-872E-01 8-481E-01 1-225E+00 4-007E+00 10 6-652E-01 9-887E-01 1-525E+00 4-416E+00 10 6-652E-01 9-987E-01 1-639E+00 4-416E+00 10 1-538E+00 10 1-639E+00 10 10 10 10 10 10 10 10 10 10 10 10 1	10 1.212E+01 1.597E+00 2.331E+00 4.966E+00 10.419E+00 2.108E+00 2.407E+00 2.42E+00 1.766E+00 5.502E+00 1.766E+00 2.467E+00 5.500E+00 10.2.467E+00 5.500E+00 10.2.467E+00 5.812E+00	10 2.011E+00 2.599F+80 3.358F+00 5.609E+00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	10 6.655E-01 1.074E+00 1.733E+00 4.515E+00 10 4.515E+00 10 4.8998E+00 2.265E+00 4.9988E+00 1.537E+00 2.265E+00 4.945E+00 10 2.240E+00 3.947E+00 5.951E+00	30 1.078E+0N 2.857E+00 4.287E+00 8.536E+00 30517E-01 6.517E-01 1.495E+00 4.313E+00 4.517E+00 4.505E+00 4.505E+00 4.505E+00 4.505E+00 4.050E+00 4.0	10 6.203E-01 9.717F-01 1.225F+01 4.050E+00 10 5.664F-01 8.330E-01 1.225F+01 4.050E+00 10 5.492F-01 8.230E-01 1.225F+01 4.057F+00 10 5.321F-01 8.074F-01 1.225F+00 4.064F+00	10 5-114F-01 7-915E-01 1-225E+00 4-071E+00 10 4-926E-01 7-768E-01 1-225E+00 4-075E+0 10 4-35E-01 1-225E+00 4-084E+0 10 1-55E+0 10 4-084E+0 10 1-225E+0 10 4-084E+0 10 10 10 10 10 10 10 10 10 10 10 10 10	10 0. 4.309E+00 10 0. 1. 4.309E+00 10 3.907E-01 6.918E-01 1.225E+09 4.119E+00 10 5.803E-01 8.431E-01 1.225F+00 4.137E+00	9.185E-01 1.434F+00 2.174E+03 5.024E+00 3.125E-101 1.486E+00 2.239F+03 5.087E+00 5.125E-101 3.621E-01 4.498F+03 6.428E+00 10.2.058E+00 3.222F+00 1.855E+03 4.18E+00 2.058E+00 3.222F+00 4.687E+00 4.817E+00 3.239E-01 1.849F+00 2.649E+03 5.08E+00 1.102E+00 1.186F+00 2.649E+03 5.08E+00 1.172F+00 1.756F+00 2.638F+03 5.08E+00
10 Z.283E-01 9.445E-01 1.225E+00 4.007E+09	10 5-872E-01 8-481E-01 1-225E+00 4-007E+00 10 6-652E-01 9-887E-01 1-525E+00 4-416E+00 10 6-652E-01 9-987E-01 1-639E+00 4-416E+00 10 1-538E+00 10 1-639E+00 10 10 10 10 10 10 10 10 10 10 10 10 1	10 1.212E+01 1.597E+00 2.331E+00 4.966E+00 10.419E+00 2.108E+00 2.407E+00 2.42E+00 1.766E+00 5.502E+00 1.766E+00 2.467E+00 5.500E+00 10.2.467E+00 5.500E+00 10.2.467E+00 5.812E+00	10 2.011E+00 2.599F+80 3.358F+00 5.609E+00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	10 6.655E-01 1.074E+00 1.733E+00 4.515E+00 10 4.515E+00 10 4.8998E+00 2.265E+00 4.9988E+00 1.537E+00 2.265E+00 4.945E+00 10 2.240E+00 3.947E+00 5.951E+00	30 1.078E+0N 2.857E+00 4.287E+00 8.536E+00 30517E+00 8.536E+00 8.517E-01 8.504E+00 4.343E+00 8.5501E-01 8.504E+00 4.043E+00 8.501E-01 8.525E+00 4.050E+00	10 6.203E-01 9.717F-01 1.225F+01 4.050E+00 10 5.664F-01 8.330E-01 1.225F+01 4.050E+00 10 5.492F-01 8.230E-01 1.225F+01 4.057F+00 10 5.321F-01 8.074F-01 1.225F+00 4.064F+00	10 5-114F-01 7-915E-01 1-225E+00 4-071E+00 10 4-926E-01 7-768E-01 1-225E+00 4-075E+0 10 4-35E-01 1-225E+00 4-084E+0 10 1-55E+0 10 4-084E+0 10 1-225E+0 10 4-084E+0 10 10 10 10 10 10 10 10 10 10 10 10 10	10 0. 4.309E+00 10 0. 1. 4.309E+00 10 3.907E-01 6.918E-01 1.225E+09 4.119E+00 10 5.803E-01 8.431E-01 1.225F+00 4.137E+00	9.185E-01 1.434F+00 2.174E+03 5.024E+00 3.125E-101 1.486E+00 2.239F+03 5.087E+00 5.125E-101 3.621E-01 4.498F+03 6.428E+00 10.2.058E+00 3.222F+00 1.855E+03 4.18E+00 2.058E+00 3.222F+00 4.687E+00 4.817E+00 3.239E-01 1.849F+00 2.649E+03 5.08E+00 1.102E+00 1.186F+00 2.649E+03 5.08E+00 1.172F+00 1.756F+00 2.638F+03 5.08E+00
18 7.283E-01 9.445E-01 1.225E+00 4.007E+09	10 5-872E-01 8-481E-01 1-225E+00 4-007E+00 10 6-652E-01 9-887E-01 1-525E+00 4-416E+00 10 6-652E-01 9-987E-01 1-639E+00 4-416E+00 10 1-538E+00 10 1-639E+00 10 10 10 10 10 10 10 10 10 10 10 10 1	10 1.212E+01 1.597E+00 2.331E+00 4.966E+00 10.419E+00 2.108E+00 2.407E+00 2.42E+00 1.766E+00 5.502E+00 1.766E+00 2.467E+00 5.500E+00 10.2.467E+00 5.500E+00 10.2.467E+00 5.812E+00	10 2.011E+00 2.599F+80 3.358F+00 5.609E+00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	10 6.655E-01 1.074E+00 1.733E+00 4.515E+00 10 4.515E+00 10 4.8998E+00 2.265E+00 4.9988E+00 1.537E+00 2.265E+00 4.945E+00 10 2.240E+00 3.947E+00 5.951E+00	30 1.078E+0N 2.857E+00 4.287E+00 8.536E+00 30517E+00 8.536E+00 8.517E-01 8.504E+00 4.343E+00 8.5501E-01 8.504E+00 4.043E+00 8.501E-01 8.525E+00 4.050E+00	10 6.203E-01 9.717F-01 1.225F+01 4.050E+00 10 5.664F-01 8.330E-01 1.225F+01 4.050E+00 10 5.492F-01 8.230E-01 1.225F+01 4.057F+00 10 5.321F-01 8.074F-01 1.225F+00 4.064F+00	10 5-114F-01 7-915E-01 1-225E+00 4-071E+00 10 4-926E-01 7-768E-01 1-225E+00 4-075E+0 10 4-35E-01 1-225E+00 4-084E+0 10 1-55E+0 10 4-084E+0 10 1-225E+0 10 4-084E+0 10 10 10 10 10 10 10 10 10 10 10 10 10	10 0. 4.309E+00 10 0. 1. 4.309E+00 10 3.907E-01 6.918E-01 1.225E+09 4.119E+00 10 5.803E-01 8.431E-01 1.225F+00 4.137E+00	9.185E-01 1.434F+00 2.174E+03 5.024E+00 3.125E-101 1.486E+00 2.239F+03 5.087E+00 5.125E-101 3.621E-01 4.498F+03 6.428E+00 10.2.058E+00 3.222F+00 1.855E+03 4.18E+00 2.058E+00 3.222F+00 4.687E+00 4.817E+00 3.239E-01 1.849F+00 2.649E+03 5.08E+00 1.102E+00 1.186F+00 2.649E+03 5.08E+00 1.172F+00 1.756F+00 2.638F+03 5.08E+00
130.00 7.283E-01 9.445E-01 1.225E+00 4.007E+09	185.00 5.872E-01 8.481E-01 1.225E+00 4.007E+00 115.00 6.552E-01 9.887E-01 1.639E+00 4.406E+00 128.00 1.639E+01 4.416E+00 128.00 1.639E+00  125.00 1.212E+UJ 1.597E+OJ 2.331E+OJ 4.966E+OJ 130.00 1.4418E+OJ 2.418RE+OJ 2.870E+OJ 5.322E+OJ 135.00 1.745E+OJ 2.407E+OJ 3.157E+OJ 5.802E+OJ 5.802E+OJ 3.736E+OJ 5.812E+OJ	1895.00 2.011E+00 2.599F+00 3.358F+00 5.609E+00 150.00 0 6.411E-01 1.041E+00 1.651E+00 4.462E+0 1.955.00 7.912E-01 1.23E+00 1.921E+00 4.656+00 1.92E-01 1.23E+00 1.92E+00 4.656+00 1.92E-01 4.656+00 1.92E-00 4.656+00 1.92E-00 1.92	155.00 6.555E-01 1.074E+00 1.733E+00 4.515E+00 175.00 175.00 4.998E+00 1.75.00 4.818E-01 1.535E+00 2.255E+00 4.998E+00 1.818.00 2.256E+00 3.21E+00 3.21E+00 3.947E+00	185.80 1.078E+UN 2.857E+UN 4.287E+DN 8.536E+DN 9.90.80 6.517E+UN 4.313E+UN 4	205.00 6.203E-01 9.717F-01 1.225F+30 4.950E+00 210.00 5.664F-01 8.30E-01 1.225F+01 4.050E+00 220.00 5.492F-01 8.202E-01 1.225F+01 4.057E+00 220.00 5.321F-01 8.074E-01 1.225F+00 4.057E+00	225.00 5.114F-01 7.915E-01 1.225F+00 4.071E+00 236.00 4.926E-01 7.58E-01 1.225E+00 4.077E+0 7.535.00 4.35E-01 7.819E-01 1.225E+00 4.084E+00 246.00 3.558E-01 6.802E-01 1.225E+00 4.084E+00	255.80 0. 0. 0. 0. 0. 0. 0. 0. 4.300E+00 0. 0. 0.300E+00 0. 0. 0.300E+00 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0	9.185F-01 1.434F+00 2.174F+03 5.024F+00 5.174F+03 5.024F+00 5.239F+03 5.087E+00 5.239F+03 5.087E+00 5.239F+03 5.087E+00 5.239F+03 5.087E+00 5.237E+03 5.087E+00 5.836F+00 5.838F+00 5.237E+00 5.237E	

Table A2. Listing of COMBCO2 Band Model Parameter Set (Cont'd)

A	 										1,,,,,,,,,	مرطر ورورو والمروروروا	
000	0000	1000C	0000	1000C	10000	0000	0000	0000	0000	9000	ko o o o	00000000000000000000000000000000000000	<b>-</b>
لتا تباليا	www	عانتانيالنان	بالماليا لماليا	عانبالبالبال	البائيا ليالبا	لعاليا ليانعا	لياليا لبالنا	لنالنالناننا	النائنانيا	بالنالناليا	للناليا ليا لياز	անանանին անանան	Ü
ᢐᢐᢐ	<b>******</b>	(C) MO C	SOMAN	らアアカ	100000	ろららろ	വ വ ക	なっている	5000	<b>ው</b> ው፡፡>	400 W CO	wouthur union	7
0 • d												nommena or	•
~∞0	თთთთ	4000	രെയയ	20 Q Q 40	Laon	3mmc	-144-44	25-	<b>տ</b> տ44	אנא נאנא	10000	nonomoranta	,
+++	++++	+++	++++	++++	+++	* + + +	++++	++++	++++	++++	++++		<b>-</b>
യാ	よらてか	<b>₩</b> •	404FV	SMON	Otot.	M 7 44	<b>~€00</b>	NOON	<b>₹</b>	らろりて	まららず	<b>るこて よらりごろしょ</b>	,
<b>∞</b> 00€	<b>BUTTO</b>	うちらん	HOMO	O M G AC		C) (D) ++1/-	23817	+ 多 こ P	2720	ntwo	11000	すれてちりをとくととと	<b>→</b>
S W												HHHHHHHHNING	
ביו כאנים	พพพพ	MMMM	mmmm	mmmm	mmmm	MMMM	2000	NONO	2000	$\alpha$	2000	<b>บบบบ</b> เบบบบบเพล	u
	0000		0000	0000	0000	8000	0000	0000	0000	0000	9000	-+++++++++	•
	անենն	نبالنائنالنا	تناليا لياليا	WHITE WAR	الناليالياليا	աևևաև	تتاليا لباليا	ساساساسا	تبانبانبانيا	بالبالباليا	யயயய	անանանականականության	J.
AUV W	000m	アりょう	( c, c c c c c c c c c c c c c c c c c c	4500	Ottor	ほうてう	നാന് തേരാ	40 44 C/1 C/1	10000	ひらす!	10284	4000000	•
•••												+4 +1 +4 +4 +4 M +4 M +4 M +4 M +4 M +4	•
CICIM	Land Code Code Code	נאנאנאנאנא	Les per per per per	ww aw	120100 <del>- 1</del>		<b>⊬</b> @₩ <b>4</b>	3100 K	2000	44 <del>44</del> 44		~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	`
200	ひひちゅ	2000	20000	0000	0000	2000	0000	6000	0000	<b>ಬರ</b> ರ	0000	<del>444</del> 4444400	7
+++	++++	++++	++++	++++	++++	++++	++++	++++	++++	++++	+++	# <b>+ + +</b> + + + + + +	
4-3(3)- 61	トシティ	M & M &	MOOG	さるとら	0000M	404	もら りて	<b>~~~</b> 010	4700	നവനമ	うしょうて	4 C C C C C C C C C C C C C C C C C C C	r
∞c⊃ 107	<b>₩©</b>	<b>SOCIO</b>	80800	らっこうら	4607	ちりょう	<b>85~~</b>	ケランク	すぐまり	ᡊᡠᢁᢂ	17+t-00	するようのできる	>
n we	พากพล	9977	~~~	~~00	יטיטיף 🕇	4mmm	ころうこく	44444	नं नं नं न	ധുകയു	~~~!	ים ים ים יון יון יון יון יון יון יון יון יון יון	i
-4-4	-1-1-1-1	स्वस्यकारा	નનનન		सम्बन्ध		च्यच्य स्त्रस	नननन				########### <b>####</b> #####################	4
+++	++++	++++	++++	++++	++++	++++	++++	++++	++++	++++	]++++	++++i+++++++	•
O-M	をてりょ	► ₹	¢C セーt(∨) チー	000h	まろりり	<b>₩</b> 00 M 00	りろうろ	4679	□ (O O ♥	ひちょう	~ さら~	๚ฅ๛๛๚๛๐๓๛๙ ๚ฅฅฅฅฅฅฅฅฅฅฅ	-
												ちょうちょうちゅうちょうちょうちょうしょうしょうしょうしょうしょうしょう	
												กล้องได้เกิดเกิดเกิดเกิดเกิดเกิดเกิดเกิดเกิดเกิด	•
ł		i							j			<del>-</del>	,
000	0000	0000	000C	0000	0000	0000	0000	0000	0000	9840	0000	++++++++	,
البنا بنيانا	ليا لنالنا لنا	<b>w</b> ww.	لما بمالتا بما	لبالبالبالبالبا	لتنانيا لتاليا	الحاليا لبائيا	لتبالعا لتالينا	كالنانناننا	التناتياتيا	لنالياناليا	النالنالناليا	recent of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control	J
4000	こうりゅひ	M 50 80 CV	$\omega \sigma m \omega$	ロタアな	1000	ちてりこ	<b>ၞ</b> ଫଫଫ	ちくりょ	9000	きょよら	60 NO	35 50 00 00 00 00 00 00 00 00 00 00 00 00	•
• • •							• • • •	· · · ·	• • • •		• • • •		•
1						1							
0000	ಐಎಐಡ	96000	0000	2000	2000	පපපස	0000	0000			0000	40000000000000000000000000000000000000	•
+++	++++ www.u	+ + + + WWW'W	4+++	++++ WWWW	++++ WU/WW	+ + + + 	나는 수 수	++++ անան	+++  ՄԱՄԱ!ԱՄ	+++ WWWW	H + + +	MMMMMMMMMM +++++++	
4401 (L)	ᡣ᠖ᠳᡚ	らて日食	യക്ഷ	<b>よら 土臼</b>	90°M	SHOH	タら まて	<b>50</b> 4€	a waw.	<b>よろのて</b>	白132~	ともしてりょうとてららりしょう	•
4474 RAI	うらてょう	N 800	5r-10	SMON	ထကက္ကတ	വനമാ	440	<b>SOMORTIN</b>	たととか	ተውውወ	することり	Hanny and and who	4
ra a	2 2 2	ttt	היחיחים	տատո	ららてて	ممجرجو			-1			<u> </u>	
+++	++++	++++	++++	++++	++++	++++	+++	++++	+ + + +	+ + + +	+ + + +	+ + + + <del> </del> + + + + <del> </del> + +	
<b>6017-00</b> 4	リアらア	りてしょ	ፍሓፍወ	$\sigma m \sim c d$	SO THOS	自とこわ	ロアタリ	$\omega\omega\omega\omega$	くこうりゅ	よるてら	りまらく	Դ <b>ՎԻՐ</b> ՄՕՄԵՐ ՄԱՄԵՐԻ ՄԵՐԻ ՄԵՐ	1
-KVMI	M 100.7	te to mm	ಎಂದಗ	~ してら	k∧.o⇔∞	6C M 440N	# (C) (C) (M)	なせる	ac ac ac le le	$o \sim \infty o$	こくよう	とまて Dプロア O78 第2	2
N+1+1	• • • •		200	المالين • • • • •	40000	പാവം	7702	~ 80 ~ G		+50.ml	11877	- www.mwa.	j
634141	HHC. H	4044	೧೯೧೦	DD44	4400	5555	0000	0000	0000	- <b>0</b>	0500	-00000000000	,
<b>\$</b>	2009	0000		<b>++</b> 11	0000		++++		+ + + +	>000 ++++	0 + + 0 + +	+++++++++	•
البالبنية	لتالياتيات	لتانتانيانا	اند ابناینانیا	اساساسانيا	الماليانا	اساساليانيا	إنبالنا نباند	البالبالبالبالنا	السانيا ايان	لبانيانيان	止いいいほ	THE POSCOCION	ı
	an oud	THO ON TO	MM &CM	സമല	► +1 \( \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot	കയത്തി	2010r	യമയസ	N eco ec cols	$v = v \circ v$	さりゅう	ひんけいり くりょうしょう	١.
40. MJ	3 ~40.01	000	1010.54			0.10.0	• • •					หนาสามพบารประชา วิเทียาสามพบาร	
ŀ	!	i		i		i i	- 1	- 1	i		I	1	
CO CI	2000	occi	0000	0000	0000					2000		20000000000000000000000000000000000000	•
Lull	1 1 + 1 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	(۱ (۱ ا سالمانمانما	1 1 + 1 WWWW			1 + + +   <b>111</b> 111111111111111111111111111111111	나 수 수 수 <b>)</b>	++++	+ + + + <u>+  </u>	+ 1 1 1 11 11 11 11 11 11 11 11 11 11 11	1 1 + 10 10 10 10 10 10 10 10 10 10 10 10 10 1	++++++	
CM-RI	T W D B	アほど見	0.4.X.X	ららって	R. P. W. O.	7 1 9 5	rocor		\$ 44.00 D	ようじょ	10八十	プラグ ちょうしゅうりょう プログラブ りゅう	•
ए के ब	coan	a wan	No.+1N	တေလ လထ		3.51-3	Sylvinia	No.44	งพงญี	1504	เกตเทา	14400000000000000000000000000000000000	
တယ် ယုံး	rwwd	<b>ന</b> മാരവ	~ ~ ~ 100	ろうせん	งดหญ	~~~~	-		mm and	40 KV	V 0 V -	merendon contractor ac	
						_~~~		~~~~		~~~			
30 G	-000									J 0 0 0			
まななる	SW SP	ខ្លួនទំនួ	2000	20,80	1. 2. 2. C.	A Ward	7,7,20	<b>17.89</b>	2000	1400	00000	rnnnrrnnnnn Lreer reese Brencrerere	
Makes becals Makes becalify	ം <b>സസ പ്ര</b> വ <b>ഡഡ</b> വ	<b>MWWW</b>	ارمه زیمه زیمه زیمه از رمه زیمه زیمه زیمه	<b>SEP 5.0</b>	24 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	N N IN IN IN IN IN IN IN IN IN IN IN IN	NWWW	New Section 1	A A TO THE	C4 C4 C4 C4 C4	100 CA CA CA CA CA CA CA CA CA CA CA CA CA	CHECK CHICK CHICK CHICK CHICK	:
i		1	,		i	1		1			ı		

_
Set (Cont'd)
Set
Parameter
Band Model
Band
g of COMBCO2 Band Mo
Listing of COMBCO2 Band
able A2.

AND SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD SEE SHOULD

· 通行经过提供可以提供的连接性经营的行用。为自然体验的产品等。

	ı		1		1		ı		1		ļ		l		1	1
MWW.	200	200	50	つうつう	2000	7 MM	164	969 C	MM CCC	MM OC	MM	MM	200	(A)(/	200	20
والمالها	1 + + 1 u u	غالنا	iu i	diant	بالباث	MALL	Řtait.	e i ka i i s	بالناأات	HIM	لماليانا	I . Ma	ltatta.		diame	141141
800	25	343	6.	10		277	7	240	200	2 (2)	80	32	96	77	200	2
c)M	∤ಌಌ	NO	100	אייסט	はいい	ろろう	1-47	-ma	<b>4</b>	400	10 4	3	<b>  ~~ ~</b>	00	100	ME
4444	410			im:		, , , , t					***		800	4+	-	44
<b>~~</b>	mm	MM	MH	777	יוכיוני	7 P7 P	*	אכאכ	N W	, hu) hu)	mm	20	2	ı٨٨	100	S
900	99	00	-	300	၁ဗာဝ	200	i co c	300	00	90	6	00	්පය	(00	60	0
نا لغالنا	تنانيا	بعالها	w	بالبالا	بالبال	عالياك	luu	بالبال	4ww	تعاليا	لنالنا	بعالها	اسس	عاندا	lww	<b>WILL</b>
400	بمازما	ろア	0.3	1000	JOH	- INM		シャン	さんの	(C) (C)	-4N	<b>自</b> 之	3	80	60	<b>C</b> C
200	4 • •	• •	•		4 •	• • 1	4 .	• •				• •	• •	• •	• • •	
<b>/~Q,</b> ←	+**	44	600	u Cue	400	non	100	)(VI+	4		4	<b>₩</b>	04	<b>~~</b>	444	+4+4
220	22	SM	200	2000	300	300	200	320	122	20	22	20	22	244	122	===
+++	++	+ +	+ 4	++	4	- 4 4	4	- 4 4		++	4+	<b>+ +</b>	++	+ +	++	++
म् जन्म	25	38	8 5 5	ノバント	122	ነመጥ	Mu	ことに	E S	90	7E	VIV M	4W	HIM MIM	3E	22
460 A		$\mathbf{m}$	<b>.</b>		41 A	1100	<b>' ' '</b>			~~		N. (1)		40	50	~m
מינימ	,	• •		• •	•	• • •	•	• • •	,	• •					901~	• •
NON			V1V	inin	1				1			-				
000	00	00		900	OC	000	COC	000		90	6	C)	00	00	CO	CO
minin	النالنا	لنالنا	MIL	غالناك	بالنال	لبالنال	liviu	بالنال	لنالنا	WILL	لنالنا	تناثنا	لناننا	لنالنا	سننا	wii
りまなり	79. 89.	44	90.4	5+4.C	44	900	933	S COL	59	<b>8</b> 1	ው ው	25	533	35	300	
0		œΝ	41		oc ∝			たんぱく	m~					91		
444		- 7	-				7 -		S		નન			4	mm	
		-1-	-4-	4+4+	4-4-	4-4-	<b>7-4</b> +	4-4-		+1+4	-4-1	-1-	44	44	4444	-40
+++	++	+ +	++	- + +	+ +	. + +	<b>  + +</b>	• + +	++	++	++	44	++	++	++	++
るとの	9E	뱃	とて	MINITE NOW-	100	. <b>(~)</b> . <b>(4</b> )	4E	1000 1000 1000 1000 1000 1000 1000 100	200	SE SE	80 CO (	1 1 1 1	20 20	WH	(1) (1) (1) (1)	TH.
9440	400	×ρΜ	20	יוני ע	ကျော	ME	ma	101	99	501	S	5	50	യഗ	th co	muj
• • •		• 4	•		• •		•		• •					• •		
NOW		- 1		-	1				1		<b>→</b> ₩1	- 1		- 1		
000	morne	~~		~~	-	,		•		~~~	~~			~~	-	
# <b>+</b> +	# + ·	++	+ Աև	+ +  W.U	+ +	+ + !!!!!!	+ + Wu	. + + ::::::::::::::::::::::::::::::::::	4 + UU	ا جا جا العاليا	## WW	+ +) 	<b>ж</b>	+ + WW	+ +  Ш Ш	+ + L(L
27E+1	290	Σď	000	3.00	50	440	20	<u> </u>	64	52	25	12	40	<u>დ</u> 0	- N	2,≪
44	41/-	1101	Ž,	16/14	2.7	200	~	144	4460	10-3	7	7	33	74	90	
ممم					1	2				-1-4	-1-1	-1-4	નન	40	منا	
806	000	ca	00	000		00	00	000	00	00	00	00	00	69	90	00
900													99		00°	
S C M	MWI MWI	البان	بالنا	باللا	WL.	LIJU.	WL	I WILL	ыÜ	ம்யூ	ww	پښ	بنين	шij	Mill More	ulu
** **	ふいん	<b>5</b> N,	S to	יא לאן ו	$ w_{\nu} $	$\sim$	00	S	444	mon	ronoi	~~~	せい	യയി	N 001	νw
60 60 M	• •	• •	• •	• •		. • •				- 4	. 4	- 4	<b>~</b> ~	- 4	with	• 4
พพน	_	ł		O.L.	ĺ	_		<b>*</b>			<b>~</b> ω.			- 1	യയ.	
000	000	200	90	00	00	00	90	50	00	00		20		00	000 000	⊃C
لنسند		. لد خ			1			است.		1		أخصنف	44	أحد		أنصف
500	0 IV 3	10	( )	34	36	57	<b>60</b> 60	30	200	-3		50	200	Nσ	900	စ္ကတ္မ
799E 659E	iv w c	2 <del>-</del>	ac	<b>60</b> ₩3	100	2000	97	24	3.0	00 cd	10 no 6	õ	NO.	29	200	7 60
		4.	<b></b>	25	7	20	2	-	444	-10	Ň÷i.		ivin.	٠,٩	1 & E	2
<b>⇔</b> +d	+0+	-10	<b>=</b> =	00	60	60	00	00	<del>-</del>	-10	C3 44 C	90	000	o d	<b></b>	-el
1.05% E + 0.0 9.934 E - 0.1 1.07% E + 0.0	000	7		+0+	0+	99	<b></b>	99	000	우루	<b>P C</b> :	25	99	25	999	29
<b>WWW</b>	بإسابيا	المار	لنالن	WIL.	min	mm	шŅ	uu	ابابيا	اليرين	إشاية	لعاليا	إخالنا	L I	إيناليا	uu
1000	Similar	o ကြိ	ž, ľ	22	0	2	0.3	r, r	800	5	Ve :	00	21	νā	-M	200
800		•	* *		017	LI CE		m = 4	TU IN	د جا ا	4	37	3/		ww.	• •
40+	Q-4-1 <b>α</b>			20	t t	we	44	+++	~ 6 (	2	40,4		+1446	M	n) (m) (m)	~-
HH H	<b>100c</b> まりす	100		7G	90	22	00	00	44.	55	Med e	57	500	20	900	>C
4 1	i i i	<u>, 4</u> ].	₩ 11111	1.4	4 +	+ +	+ +	++	ĮŢ.		i i	1 1	1 1	+ +	4 4 i	+ +
400	L.V.	N	200	22	36	179	20	50	300	Ď,	-101	7.00	200	7.7	あた。 でこ。	2
722	70 to 10	:2:	<b>⇒4</b>	501	いら	44		50	400	24	<b>Σ</b> ,600 ε 1,1ω, (	įΩ,	400	YE!	6 4 F	NIC.
7.724E-01 7.576E-01 7.795E-01	 	;4,	44	8:4	24	-12		لبنا	'nů,	ئىن.	 	600		<b>.</b>	e .	• 4
000	- -	. ا	> r=	ا ا		60	00	-	ි සුපුද	200	- cac	3C1	56	ا م	<u></u>	3
36.00	900	-	200	~ E	<u>ė</u> ė	64	<u> </u>	က်မ	000	-9	၁ထိ	50	50	20	وقو	e:
200	VEN	S	Ϋ́	ďΞ	Řά	ν̈́Ξ	νõ	ХŒ	ŘΒí	र्व	أجأر		ŽΑ̈́	(d	Ϋ́ĕ́	7
200	٤		o do	20	9	العاق	ي و	200	ر ا		-6-6	-				-
4-2 Cal Cal	) (m) (m)	· m	الرجنا ل	La led	الماسما	L. POR	زيمة دما	in)	ins less in	ונאניי	7 (VI) (V	ו ניוני	*) <b>(*)</b> (*)	-	*7 <b>#</b> 7 #	ריאני

TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITILLITI

THE TILLITI

 SELF-BROADENING NON-RESC adamadanadan a 

ouestaintrussa werthaltrosamon wertsassassassa weresassassassassa minimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimuminimumi

๛๎๛๛๛๛๛๛๛๛๛๛ ๛๛๛๛๛๛๛๛๛๛๛๛

#### LABORATORY OPERATIONS

是是各种的一种,但是他们是一种,但是是一种,他们也是是一种,他们也是一种的,他们也是一种的,他们也是一种的人,也是一种的人,也是一种的人,也是一种的人,也是一种的人,

The Laboratory Operations of The Aerospace Corporation is conducting experimental and theoretical investigations necessary for the evaluation and application of scientific advances to new military concepts and systems. Versatility and flexibility have been developed to a high degree by the laboratory personnel in dealing with the many problems encountered in the nation's rapidly developing space and missile systems. Expertise in the latest scientific developments is vital to the accomplishment of tasks related to these problems. The laboratories that contribute to this research are:

Aerophysics Laboratory: Launch and reentry aerodynamics, heat transfer, reentry physics, chemical kinetics, structural mechanics, flight dynamics, atmospheric pollution, and high-power gas lasers.

Chemistry and Physics Laboratory: Atmospheric reactions and atmospheric optics, chemical reactions in polluted atmospheres, chemical reactions of excited species in rocket plumes, chemical thermodynamics, plasma and laser-induced reactions, laser chemistry, propulsion chemistry, space vacuum and radiation effects on materials, lubrication and surface phenomena, photosensitive materials and sensors, high precision laser ranging, and the application of physics and chemistry to problems of law enforcement and biomedicine.

Electronics Research Laboratory: Electromagnetic theory, devices, and propagation phenomena, including plasma electromagnetics; quantum electronics, lasers, and electro-optics; communication sciences, applied electronics, semiconducting, superconducting, and crystal device physics, optical and acoustical imaging; atmospheric pollution; millimeter wave and far-infrared technology.

Materials Sciences Laboratory: Development of new materials; metal matrix composites and new forms of carbon; test and evaluation of graphite and ceramics in reentry; spacecraft materials and electronic components in nuclear weapons environment; application of fracture mechanics to stress corrosion and fatigue-induced fractures in structural metals.

Space Physics Laboratory: Atmospheric and ionospheric physics, radiation from the atmosphere, density and composition of the atmosphere, aurorae and airglow; magnetospheric physics, cosmic rays, generation and propagation of plasma waves in the magnetosphere; solar physics, studies of solar magnetic fields; space astronomy, x-ray astronomy; the effects of nuclear explosions, magnetic storms, and solar activity on the earth's atmosphere, ionosphere, and magnetosphere; the effects of optical, electromagnetic, and particulate radiations in space on space systems.

THE AEROSPACE CORPORATION El Segundo, California